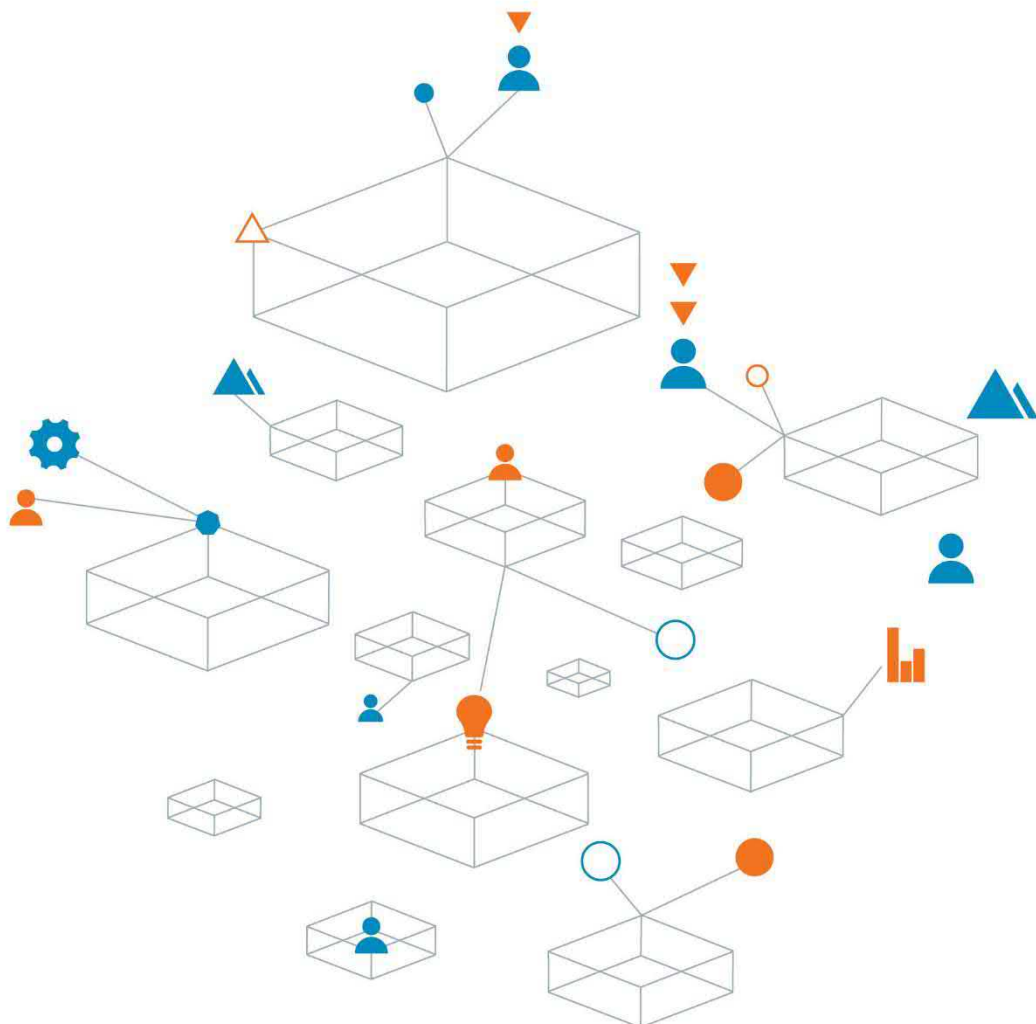


Appendix 9: Geotechnical Report

9 March 2021



Trust is the
cornerstone
of all our
projects

Birch's Village Plan Change

Prepared for
Birch's Village Limited

Prepared by
Coffey Services (NZ) Limited
1/254 Montreal Street
Christchurch Central City
8013 New Zealand
t: +64 3 374 9600 f: +64 3 374 9601
NZBN 9429033691923

9 March 2021

773 CHCGE283773

Quality information

Revision history

Revision	Description	Date	Originator	Reviewer	Approver
V0	GAR	09/03/2021	AJ	RB	AJ

Distribution

Report Status	No. of copies	Format	Distributed to	Date
Final	1	PDF	Sally Eldford (Baseline Group)	09/03/2021

Table of contents

1. Introduction.....	1
2 Scope	1
3. Proposed development	1
4 Publicly available geotechnical data (NZGD)	2
5. Coffey site investigation	3
6 Site performance	4
6.1. Ground motion	4
7 Ground model	5
7.1. Geology	5
7.2 Groundwater	5
7.3. Investigation findings.....	5
7.4 Site sub soil class	6
8. Geotechnical hazard assessment	6
8.1 Erosion	6
8.2. Falling debris	6
8.3 Subsidence	6
8.3.1. Liquefaction induced settlement.....	6
8.3.2 Free-field settlements	6
8.3.3. Static settlement	7
8.4 Slippage	7
8.5. Inundation.....	7
9 Conclusions	8
10. Limitations	8
11 Closure	9

Tables

Table 1: NZGD investigation summary

Table 2: Coffey investigation summary

Table 3: Ground profile

Table 4: Estimated “free-field” post-liquefaction ground surface settlements and Technical Category

Appendices

Appendix A - Site plan and factual data

Appendix B Liquefaction analysis

1. Introduction

Birch's Village Limited has engaged Coffey Services (NZ) Limited to carry out a geotechnical investigation and assessment of suitability for a proposed Plan Change and future subdivision at 57 Hamptons Road and 142 to 214B Birchs Road, Prebbleton, about 4.5 km south of Hornby, Canterbury. The purpose of this report is to support a Plan Change application for the construction of new residential Lots at the site.

Our assessment has considered the items required by Section 106 of the RMA. In our opinion the site is considered geotechnically suitable for subdivision subject to further investigation and design at the subdivision consent stage.

2. Scope

An investigation methodology for the 42.3 Ha site was developed and carried out by Coffey, as outlined below:

- Review of previous geotechnical investigations including previous work on the site and surrounding area.
 - This identified 3 existing CPTs on the site and 1 borehole
- Site walkover to assess geotechnical hazards
- Completion of 8 new piezocone penetration tests (CPTs). The CPT tests are a primary investigation tool used to develop the preliminary ground model at the site.
- 2 hand augered boreholes were also undertaken to check topsoil depth and confirm the depth to ground water.
- Assessment of the geotechnical hazards at the site per Section 106 of the RMA.
- Geotechnical analyses and reporting.

Coffey have considered the following in the preparation of this report:

- Existing geotechnical investigation data available in the area from the New Zealand Geotechnical Database (NZGD)
- The new geotechnical investigations data
- Project correspondence with the wider Plan Change by Birch's Village Limited

Reference has also been made to the MBIE Guidance Part D: Subdivisions, to confirm that the requirements outlined in these documents have been incorporated in this report.

3. Proposed development

The proposed Plan Change area comprises a series of 9 land parcels totalling 42.3 Ha located to the south of Prebbleton. The site is made up by a number of lifestyle properties which comprise large areas of greenfield land with localised residential houses (see the Site Plan, Figure 1 below).



Figure 1: Site plan

4. Publicly available geotechnical data (NZGD)

As part of our desktop study review we identified four site specific deep investigation data points and eight site specific shallow data points. These investigations have been summarised in Table 1 below and have been used as part of our assessment of the site. The factual information from each of these tests (including site location plan) is presented in Appendix A of this report.

Table 1: NZGD investigation summary

Reference	Date of test	Depth of test (metres below ground level)	Depth to groundwater (as measured)	Termination criteria
BH-35576	17/10/2013	~20.0	~2.0	Target depth
CPT-115979	13/11/2017	~3.7	Not measured	Effective refusal
CPT-88221	14/10/2016	~12.3	Not measured	Effective refusal
CPT-88224	14/10/2016	~9.3	Not measured	Effective refusal
KGA HA01	13/11/2017	~0.8	Not measured	Effective refusal
KGA – HA02	13/11/2017	~1.0	Not measured	Effective refusal
KGA HA03	13/11/2017	~3.0	Not measured	Target depth
KGA – HA04	13/11/2017	~1.0	Not measured	Effective refusal
KGA HA05	13/11/2017	~3.0	Not measured	Target depth
KGA – HA06	13/11/2017	~3.0	Not measured	Target depth
KGA HA07	13/11/2017	~3.0	Not measured	Target depth
KGA – HA08	13/11/2017	~3.0	Not measured	Target depth

5. Coffey site investigation

Coffey completed additional testing across the site in order to geotechnically characterise the site. This testing was targeted to generating a generalised ground model across the site for the purpose of resource consent application. We completed the investigation based on land access, and note that we did not access two properties on the SE part of the site (see Site Plan in Appendix A). We note that some additional infill investigation may be required in this area prior to final subdivision consent being granted.

The testing was completed on 12 February 2021 and is summarised in Table 2 below. The logs and sub-surface information from each of these tests (including site location plan) is presented in Appendix A of this report.

Table 2: Coffey investigation summary

Reference	Depth of test (metres below ground level)	Depth to groundwater [m] (as measured)	Termination criteria
HA1	~2.0	Not encountered	Target depth
HA2	~1.5	Not encountered	Effective refusal
CPT-01	~2.4	Not measured	Effective refusal
CPT-02	~6.7	Not measured	Effective refusal
CPT-03	~4.8	Not measured	Effective refusal
CPT-04	~1.5	Not measured	Effective refusal
CPT-05	~4.0	Not measured	Effective refusal
CPT-06	~2.3	Not measured	Effective refusal
CPT-07	~2.1	Not measured	Effective refusal
CPT-08	~1.8	Not measured	Effective refusal

6. Site performance

6.1. Ground motion

Using the MBIE¹ and Bradley & Hughes (2012)¹ procedures, we have found that the site was “sufficiently tested” to the Serviceability Limit State (SLS) level of earthquake demand during the 4 September 2010, 22 February 2011 and 13 June 2011 earthquake events of the CES. We note that in Prebbleton the 4 September M7.1 Darfield Earthquake caused stronger and longer duration ground shaking than the 22 February Christchurch Earthquake.

An assessment has been made regarding predicted earthquake induced deformation that may occur in a design earthquake based on geological setting, site terrain, and the level of “test” previously experienced. It is considered that:

- An SLS earthquake event is likely to cause less damage to that experienced in the 4 September 2010 earthquake and to be similar to the February 2011 earthquake.
- Under ultimate limit state (ULS) conditions, the nature of land and building damage is likely to be similar to that already experienced in the 4 September 2010 earthquake of the CES.

¹ Bradley & Hughes (2012) *Conditional Peak Ground Accelerations in the Canterbury Earthquakes for Conventional Liquefaction Assessment*. Report for DBH (MBIE), April 2012.

7. Ground model

7.1. Geology

The geological map² of the area indicates that the site is underlain by "Grey to brown alluvium, comprising silty sub-angular gravel and sand forming alluvial fans (Q1a)" (also known as alluvium) of the Springston Formation.

7.2. Groundwater

The shallow ground investigation completed by KGA at the site assumed a ground water of approximately 0.9mbgl based on an inference from the CPT test undertaken at the site. These same tests logged soils as dry to moist to the test termination at 3.0mbgl in some instances. This indicates that standing ground water is not present at the 0.9mbgl that is assumed by KGA in their shallow HA tests.

BH 35576 recorded a standing ground water depth at approximately 2.0mbgl and Coffey's two shallow HA boreholes undertaken on 12 February 2021 did not encounter groundwater within the upper 1.5 to 2.0m of the soil profile. Based on this evidence it is likely that the water level recorded in BH 35576 is likely to be a perched water level from drilling.

Based on the above we consider it appropriate to assume a conservative ground water depth of 2.0mbgl, although we anticipate that over the majority of the site the ground water may be present at greater than 3.0mbgl.

7.3. Investigation findings

Eleven CPTs, eight HA, and one deep borehole test have been used to develop the ground model for the Birch's Village subdivision. A summary of the ground model is provided below:

Table 3: Ground profile

Description		Strength/consistency	Thickness (m)	Depth to top of layer (mbgl)
Springston Formation	Sandy silt and organic silt (topsoil)		0.3 to 0.4	0.0
	Interbedded alluvium: Silt, sand, sandy silt and silty sand	Typically: Firm to stiff / loose to dense	Majority of site: 1.5 to 4.5 Mid-eastern side: up to 9.0	0.3 to 0.4
	Interbedded alluvium: typically sand and gravel deposits with some layers of silt, sandy silt and silty sand	Medium dense to very dense, non-liquefiable	>20m	1.5 to 9.0

The above ground profile is simplified as an illustration; however, the actual ground profile includes a highly interbedded (interfingering) layering of silty alluvium and sandy alluvium overlying a dense to very dense gravel layer. These sand and silt layers are typically inorganic and have moderate strength properties. We note that the area surrounding BH 35567 has appears to have a deeper silt /

² Forsyth, P.J.; Barrell, D.J.A.; Jongens, R. (compilers) 2008: Geology of the Christchurch area: scale 1:250,000. Lower Hutt: GNS Science. Institute of Geological & Nuclear Sciences 1:250,000 geological map 16. 67 p. + 1 folded map

sand profile (up to 9.0mbgl) when compared to the remainder of the site where shallow refusal of the CPT tests typically occurred at depths shallower than 4.5mbgl

7.4. Site sub-soil class

In accordance with NZS1170.5, Section 3.1.3, a subsoil classification of "Class D – Deep or soft soil sites" can be assumed for the site.

8. Geotechnical hazard assessment

8.1. Erosion

The site has relatively flat topography and is bounded by grassed paddock land. Provided appropriate stormwater systems are installed as part of the development, there will be few viable sources of erosion at this site.

8.2. Falling debris

As there are no slopes or exposed hills or rock faces surrounding the site, there are no sources of falling debris at the site, or for the surrounding area.

8.3. Subsidence

8.3.1. Liquefaction induced settlement

ECAN Technical Report: Review of liquefaction hazard in eastern Canterbury, including Christchurch City and parts of Selwyn, Waimakariri and Hurunui Districts describes the sites as falling near the boundary of the mapped "*Damaging liquefaction unlikely*" and "*Liquefaction assessment needed*". Given the site's zoning we consider it unlikely that liquefaction would be a significant hazard at the site; however, we have undertaken analyses which record the following:

SLS and ULS design earthquake scenarios are assessed using the parameters provided by the MBIE Guidance for an Importance Level 2 (IL2) structure and a Class D subsoil site.

The liquefaction triggering analysis was carried out for the CPTs shown on the site plan (Appendix A) using the Boulanger and Idriss (2014) method³ and proprietary liquefaction assessment software⁴, in accordance with the updates to the MBIE Guidance¹ (Issue 7 October 2014).

8.3.2. Free-field settlements

The type of settlement that is most commonly estimated when liquefaction analysis is conducted (refer to Section 6.3) is referred to as the *free-field settlement*. Free-field settlement is the component of land settlement that does not take account of foundation influences (e.g. loads and stiffness), or the effects of ground loss, lateral spread, strength degradation, sand ejecta and ground cracks.

According to the MBIE Guidance, an "Index Value" for categorising future expected land performance can be assigned by analysing the upper 10m of the soil profile. The rationale for this is that liquefaction in the upper 10m of the profile is known to be most manifested at the ground surface.

³ Boulanger, R.W., Idriss, I.M., CPT and SPT liquefaction triggering procedures, Report No. UCD/CGM-14/01, April 2014, Centre for Geotechnical Modelling, Department of Civil and Environmental Engineering at the University of California, Davis, California

⁴ Geologismiki Geotechnical Software, CLiq v.3.0.3.2 – CPT Liquefaction Assessment Software

Where CPTs refused before 10m, we have assessed the predicted values to be representative of the site due to the density and consistency of the refusal layer across the site and in BH 35576

The estimated free-field settlement values and the correlated residential foundation Technical Category, as defined by Table 3 1 of the MBIE Guidance, are given in Table 4

Table 4: Estimated "free-field" post-liquefaction ground surface settlements and Technical Category

CPT Location	Termination Depth (mbgl)	Free-field settlements to refusal depth (mm)		MBIE Technical Category
		SLS	ULS	
CPT01	~2.4	<5	<5	TC1
CPT02	~6.7	<5	<15	TC1
CPT03	~4.8	<10	<50	TC2
CPT04	~1.5	<5	<5	TC1
CPT05	~4.0	<5	<30	TC2
CPT06	~2.3	<5	<5	TC1
CPT07	~2.1	<5	<5	TC1
CPT08	~1.8	<5	<5	TC1
CPT-115979	~3.7	<5	<30	TC2
CPT-88221	~12.3	<45	<80	TC2
CPT-88224	~9.3	<35	<95	TC2

The CPT analyses show that the site is predominantly TC1-like with small areas that contain TC2-like ground. This is generally in accordance with the ECan technical report referenced in Section 8.3.1 of this report. It appears that liquefaction was not observed in the site area following the most severe 2010 Darfield Earthquake, which indicates that liquefaction at the site is unlikely in strong earthquake shaking.

Dependent on the desired TC classifications for the development it may be beneficial to the development to conduct additional CPT testing to maximise the amount of land deemed suitable for TC1 foundations. This additional investigation could be completed if needed at subdivision consent stage.

8.3.3. Static settlement

The ground investigation data at the site suggested that the site soils are generally inorganic in nature. Based on this information we consider that the risk of static settlements across the site could be managed through normal residential construction practices such as proof compacting the base of foundation excavations.

8.4. Slippage

We have not observed any sources of land instability on the site and due to the flat site topography, we consider the risk of slope failure to be very low. The appropriate design of batter slopes near waterways will mitigate this risk further.

8.5. Inundation

In relation to stormwater inundation, we recommend that drainage design and management be addressed by specialist consultants as it is beyond the scope of this report. We expect that with appropriate stormwater and flood control systems, the risk of inundation will be low.

9. Conclusions

The overall site is well covered with CPT probes and other geotechnical investigations. Based on the on-site testing carried out to date, the majority of the site is TC1 like with some minor pockets of TC2 like performance. This categorisation is generally in line with the ECan mapping of the site which places it on the boundary of an area where liquefaction assessment is required and an area where damaging liquefaction is unlikely.

We consider that the site is suitable for residential development subject to further investigation and design at the subdivision consent stage.

Additional geotechnical investigation may be required to refine the technical categories for the proposed Lots once a subdivision plan has been further developed. We also recommend that a groundwater monitoring programme is implemented to allow for more accurate liquefaction analyses

10. Limitations

This report has been prepared solely for the use of our client, Birch's Village Limited, their professional advisers and Selwyn District Council (SDC) in relation to the specific project described herein. No liability is accepted in respect of its use for any other purpose or by any other person or entity.

It is recommended that all other parties seek professional geotechnical advice to satisfy themselves as to its on-going suitability for their intended use.

As subsurface information has been obtained from discrete investigation locations, which by their nature only provide information about a relatively small volume of subsoils, there may be special conditions pertaining to this site which have not been disclosed by the investigation and which have not been taken into account in the report. If variations in the subsoils occur from those described or assumed to exist, then the matter should be referred to us immediately.

Please also refer to the enclosed *Important Information about Your Coffey Report*.

11. Closure

If you have queries or require further clarification regarding aspects of this report, please contact the undersigned

For and on behalf of Coffey

Prepared by

Andrew Jordan

Senior Engineering Geologist

Reviewed by

Richmond Beetham

BSc MSc Eng BE CEngNZ CPEng PEngGeol
Principal Geotechnical Engineer

Important information about your Coffey Report

As a client of Coffey you should know that site subsurface conditions cause more construction problems than any other factor. These notes have been prepared by Coffey to help you interpret and understand the limitations of your report.

Your report is based on project specific criteria

Your report has been developed on the basis of your unique project specific requirements as understood by Coffey and applies only to the site investigated. Project criteria typically include the general nature of the project; its size and configuration; the location of any structures on the site; other site improvements; the presence of underground utilities; and the additional risk imposed by scope-of-service limitations imposed by the client. Your report should not be used if there are any changes to the project without first asking Coffey to assess how factors that changed subsequent to the date of the report affect the report's recommendations. Coffey cannot accept responsibility for problems that may occur due to changed factors if they are not consulted.

Subsurface conditions can change

Subsurface conditions are created by natural processes and the activity of man. For example, water levels can vary with time, fill may be placed on a site and pollutants may migrate with time. Because a report is based on conditions which existed at the time of subsurface exploration, decisions should not be based on a report whose adequacy may have been affected by time. Consult Coffey to be advised how time may have impacted on the project.

Interpretation of factual data

Site assessment identifies actual subsurface conditions only at those points where samples are taken and when they are taken. Data derived from literature and external data source review, sampling and subsequent laboratory testing are interpreted by geologists, engineers or scientists to provide an opinion about overall site conditions, their likely impact on the proposed development and recommended actions. Actual conditions may differ from those inferred to exist, because no professional, no matter how qualified, can reveal what is hidden by earth, rock and time. The actual interface between materials may be far more gradual or abrupt than assumed based on the facts obtained. Nothing can be done to change the actual site conditions which exist, but steps can be taken to reduce the impact of unexpected conditions. For this reason, owners should retain the services of Coffey through the development stage, to identify variances, conduct additional tests if required, and recommend solutions to problems encountered on site.

Your report will only give preliminary recommendations

Your report is based on the assumption that the site conditions as revealed through selective point sampling are indicative of actual conditions throughout an area. This assumption cannot be substantiated until project implementation has commenced and therefore your report recommendations can only be regarded as preliminary. Only Coffey, who prepared the report, is fully familiar with the background information needed to assess whether or not the report's recommendations are valid and whether or not changes should be considered as the project develops. If another party undertakes the implementation of the recommendations of this report there is a risk that the report will be misinterpreted and Coffey cannot be held responsible for such misinterpretation.

Your report is prepared for specific purposes and persons

To avoid misuse of the information contained in your report it is recommended that you confer with Coffey before passing your report on to another party who may not be familiar with the background and the purpose of the report. Your report should not be applied to any project other than that originally specified at the time the report was issued.

Interpretation by other design professionals

Costly problems can occur when other design professionals develop their plans based on misinterpretations of a report. To help avoid misinterpretations, retain Coffey to work with other project design professionals who are affected by the report. Have Coffey explain the report implications to design professionals affected by them and then review plans and specifications produced to see how they incorporate the report findings.

Data should not be separated from the report

The report as a whole presents the findings of the site assessment and the report should not be copied in part or altered in any way. Logs, figures, drawings, etc. are customarily included in our reports and are developed by scientists, engineers or geologists based on their interpretation of field logs (assembled by field personnel) and laboratory evaluation of field samples. These logs etc. should not under any circumstances be redrawn for inclusion in other documents or separated from the report in any way.

Geoenvironmental concerns are not at issue

Your report is not likely to relate any findings, conclusions, or recommendations about the potential for hazardous materials existing at the site unless specifically required to do so by the client. Specialist equipment, techniques, and personnel are used to perform a geoenvironmental assessment. Contamination can create major health, safety and environmental risks. If you have no information about the potential for your site to be contaminated or create an environmental hazard, you are advised to contact Coffey for information relating to geoenvironmental issues.

Rely on Coffey for additional assistance

Coffey is familiar with a variety of techniques and approaches that can be used to help reduce risks for all parties to a project, from design to construction. It is common that not all approaches will be necessarily dealt with in your site assessment report due to concepts proposed at that time. As the project progresses through design towards construction, speak with Coffey to develop alternative approaches to problems that may be of genuine benefit both in time and cost.

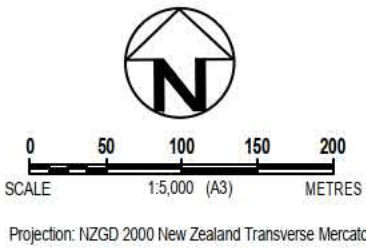
Responsibility

Reporting relies on interpretation of factual information based on judgement and opinion and has a level of uncertainty attached to it, which is far less exact than the design disciplines. This has often resulted in claims being lodged against consultants, which are unfounded. To help prevent this problem, a number of clauses have been developed for use in contracts, reports and other documents. Responsibility clauses do not transfer appropriate liabilities from Coffey to other parties but are included to identify where Coffey's responsibilities begin and end. Their use is intended to help all parties involved to recognise their individual responsibilities. Read all documents from Coffey closely and do not hesitate to ask any questions you may have.

Appendix A - Site plan and factual data



revision	no.	description			drawn	approved	date
	A	ORIGINAL ISSUE			RZ	AJ	08.03.21



drawn	RZ
approved	AJ
date	08.03.2021
scale	AS SHOWN
original size	A3



client:		BIRCH'S VILLAGE LIMITED		
project:		BIRCH'S VILLAGE, PREBBLETON		
title:		SITE PLAN		
project no:		773-CHCGE283773	figure no:	01
			rev:	A

MXD ref: 283773_01_GS001_1

Engineering Log - Hand Auger

client: **Birche's Village Limited**

principal: -

project: **Geotechnical Assessment Report for Plan Change**

location: **Birch's Village, Birchs Road, Prebbleton**

Borehole ID: **HA1**

sheet: 1 of 1

project no. **773-CHCGE283773**

date started: **12 Feb 2021**

date completed: **12 Feb 2021**

logged by: **B. Chau**

checked by: **A. Jordan**

position: Not Specified surface elevation: Not Specified angle from horizontal: 90°
drill model: Hand Auger drilling fluid: - hole diameter: 50 mm

drilling information					material substance				
method & support	penetration	water	samples & field tests	RL (m)	depth (m)	graphic log	classification symbol	material description SOIL TYPE: plasticity or particle characteristic, colour, secondary and minor components	moisture condition
HA N	1	Not Encountered					ML	Sandy SILT: non plastic - low plasticity, pale brown, with trace of rootlets.	D
	2				0.5		ML	SILT: low plasticity, yellow-brown with orange and grey staining, with some fine grained sand.	M
	3				1.0				
					1.5			1.7 to 1.8 m: grey SILT with some fine grained sand	
					2.0		SM	SILTY SAND: fine grained, low plasticity, yellow-brown. Hand Auger HA1 terminated at 2.0 m Target depth	
					2.5				
					3.0				
					3.5				

method AD auger drilling* AS auger screwing* HA hand auger W washbore HA hand auger	support M mud C casing N nil	penetration 	samples & field tests B bulk disturbed sample D disturbed sample E environmental sample SS split spoon sample U## undisturbed sample ##mm diameter HP hand penetrometer (kPa) N standard penetration test (SPT) N* SPT - sample recovered Nc SPT with solid cone VS vane shear; peak/remoulded (kPa) R refusal HB hammer bouncing	classification symbol & soil description based on Unified Classification System	consistency / relative density VS very soft S soft F firm St stiff VSt very stiff H hard Fb friable VL very loose L loose MD medium dense D dense VD very dense
moisture D dry M moist W wet Wp plastic limit WL liquid limit					

* bit shown by suffix
e.g.
AD/T
B blank bit
T TC bit
V V bit

client: **Birche's Village Limited**

principal: -

project: **Geotechnical Assessment Report for Plan Change**

location: **Birch's Village, Birchs Road, Prebbleton**

Borehole ID. **HA2**

sheet: 1 of 1

project no. **773-CHCGE283773**

date started: **12 Feb 2021**

date completed: **12 Feb 2021**

logged by: **B. Chau**

checked by: **A. Jordan**

position: Not Specified

surface elevation: Not Specified

angle from horizontal: 90°

drill model: Hand Auger

drilling fluid: -

hole diameter : 50 mm

drilling information					material substance								
method & support	penetration		water	samples & field tests	RL (m)	depth (m)	graphic log	classification symbol	material description SOIL TYPE: plasticity or particle characteristic, colour, secondary and minor components	moisture condition	consistency / relative density	hand penetrometer (kPa)	structure and additional observations
	1	2											
<div><div>HA</div><div>N</div></div>	1	2	Not Encountered			0.5		ML	Sandy SILT: low plasticity, brown, with trace of rootlets.	D			TOPSOIL
								SP	SAND: fine grained, yellow-brown with some orange mottling, and some silt.	M		SPRINGSTON FORMATION	
						1.5			1.45 m: trace to some medium to coarse grained, subrounded gravel. Hand Auger HA2 terminated at 1.45 m Refusal				
						2.0							
						2.5							
						3.0							
						3.5							

method

AD auger drilling*

AS auger screwing*

HA hand auger

WA washbore

HA hand auger

support

M mud

C casing

penetration

water

10-Oct-12 water level on date shown

water inflow

water outflow

samples & field tests

B bulk disturbed sample

D disturbed sample

E environmental sample

SS split spoon sample

U## undisturbed sample ##mm diameter

HP hand penetrometer (kPa)

N standard penetration test (SPT)

N* SPT - sample recovered

Nc SPT with solid cone

VS vane shear, peak/remoulded (kPa)

R refusal

HB hammer bouncing

classification symbol & soil description

based on Unified Classification System

moisture

D dry

M moist

W wet

Wp plastic limit

WI liquid limit

consistency / relative density

VS very soft

S soft

F firm

St stiff

VSt very stiff

H hard

Fb friable

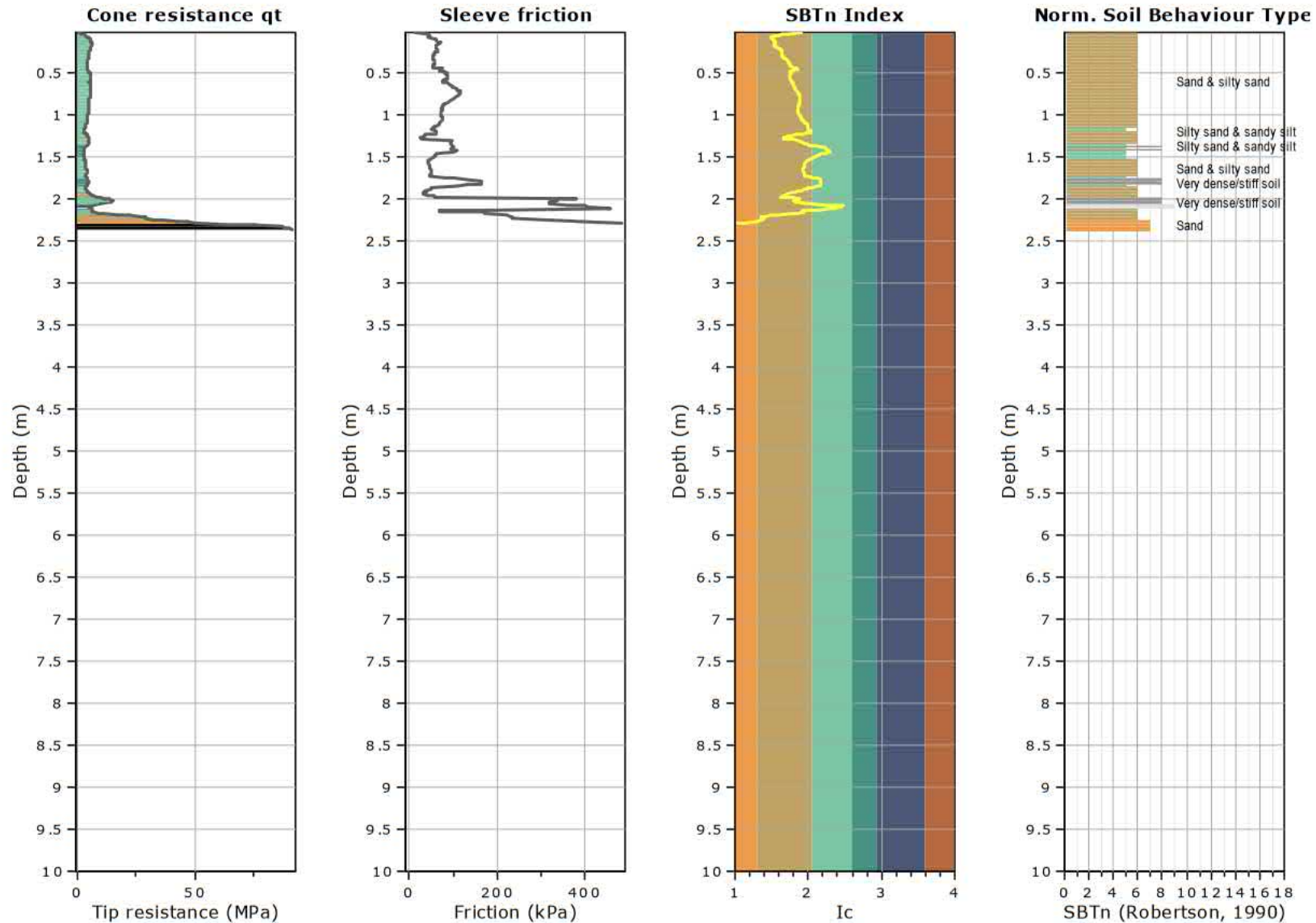
VL very loose

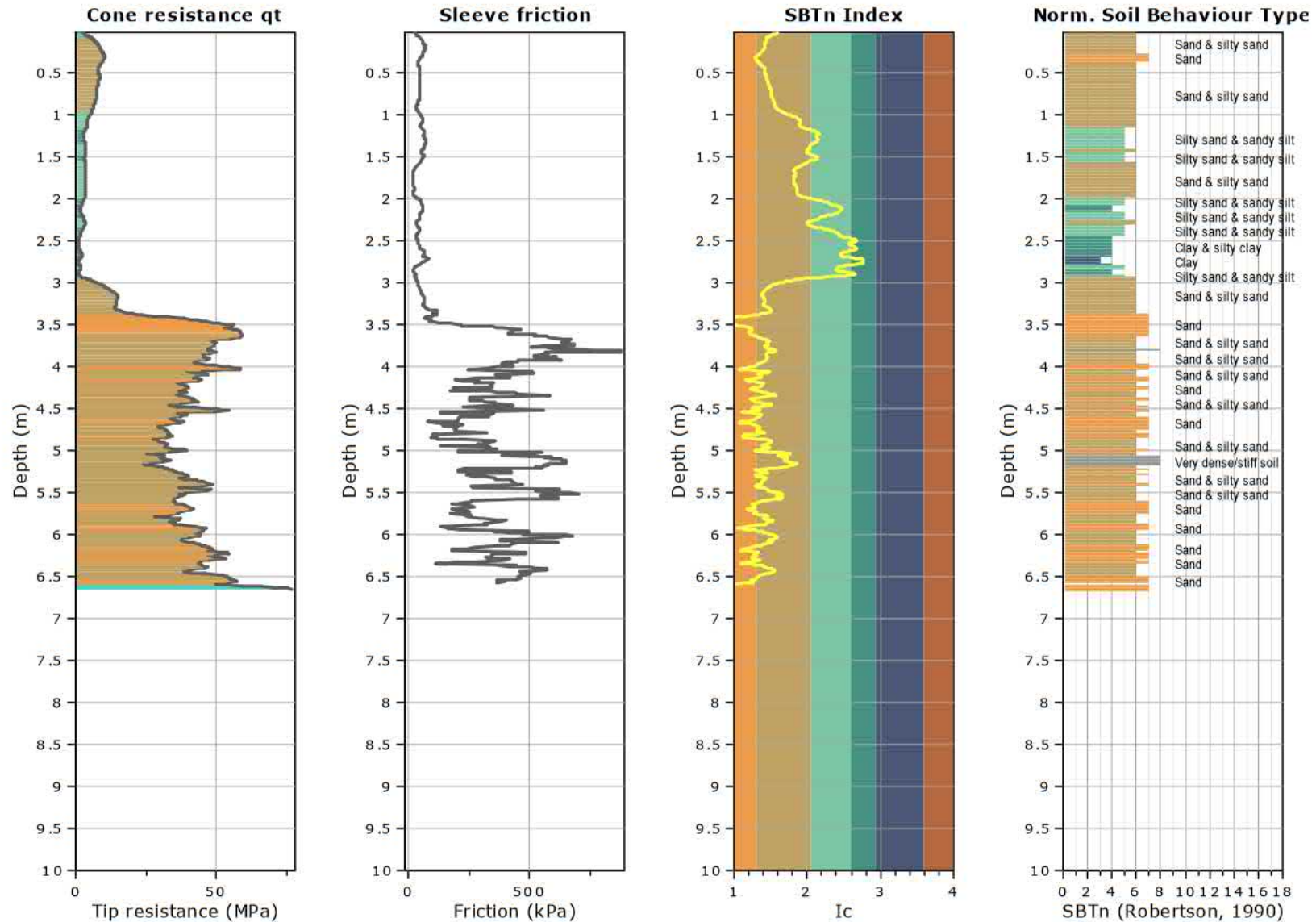
L loose

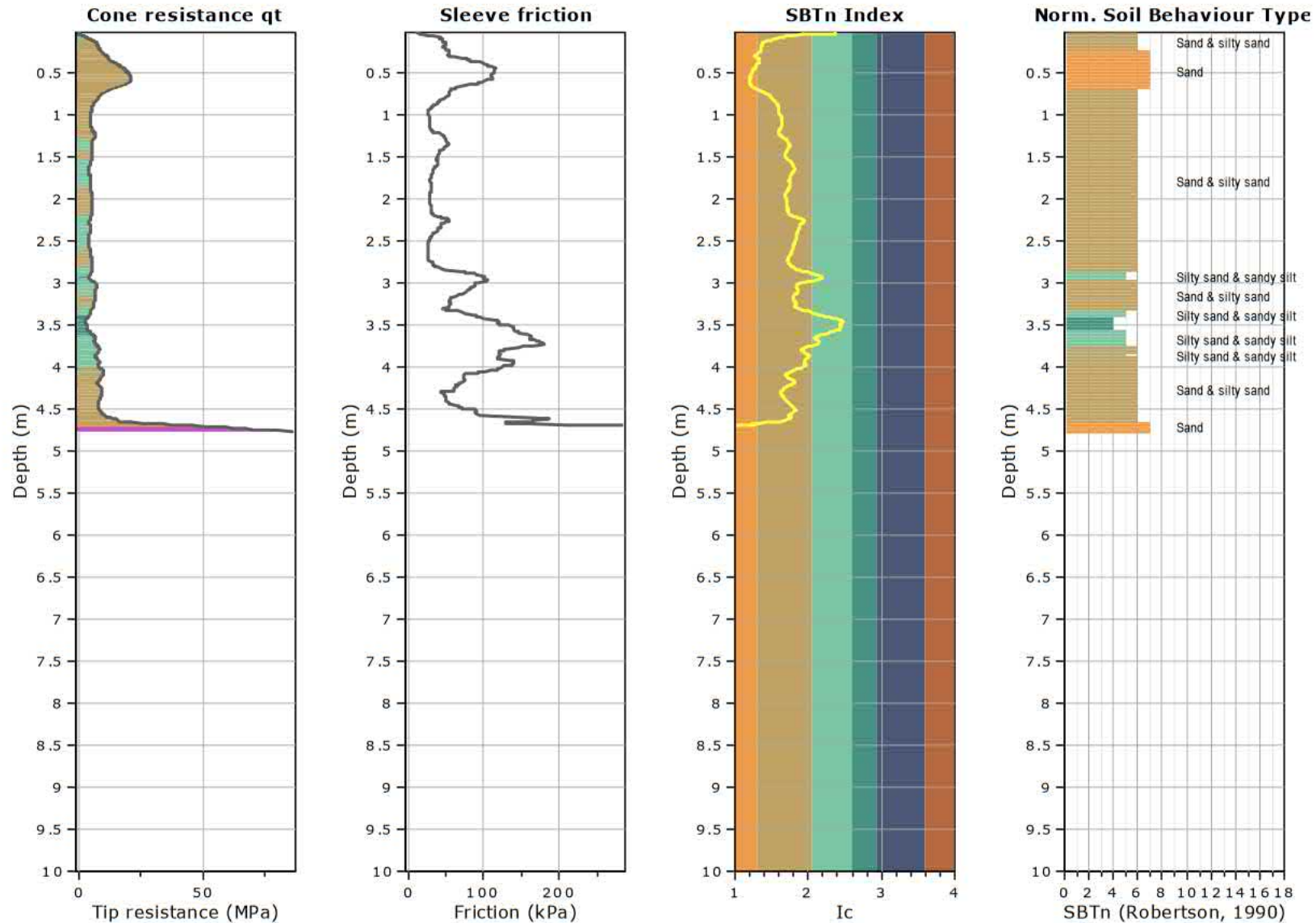
MD medium dense

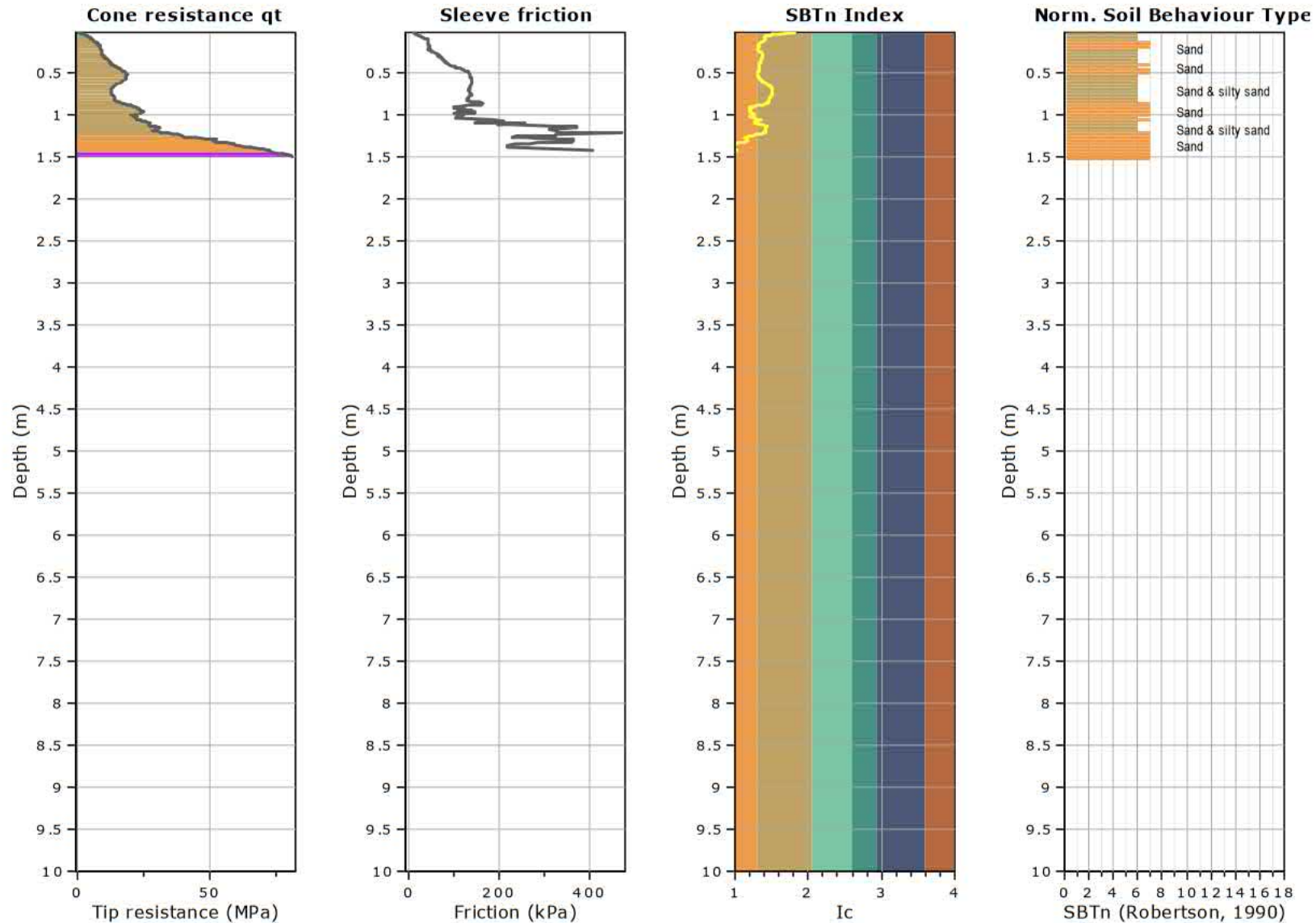
D dense

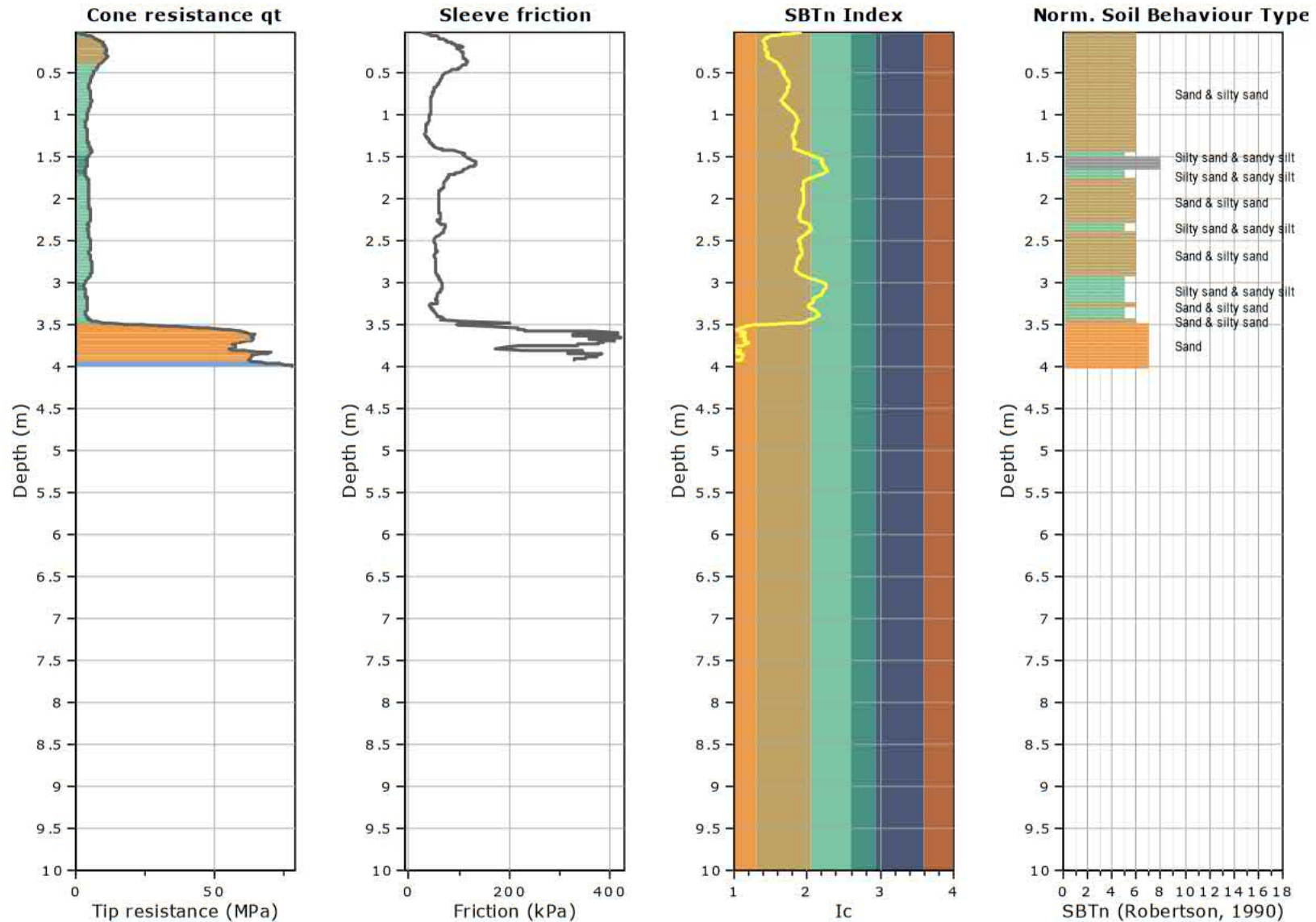
VD very dense

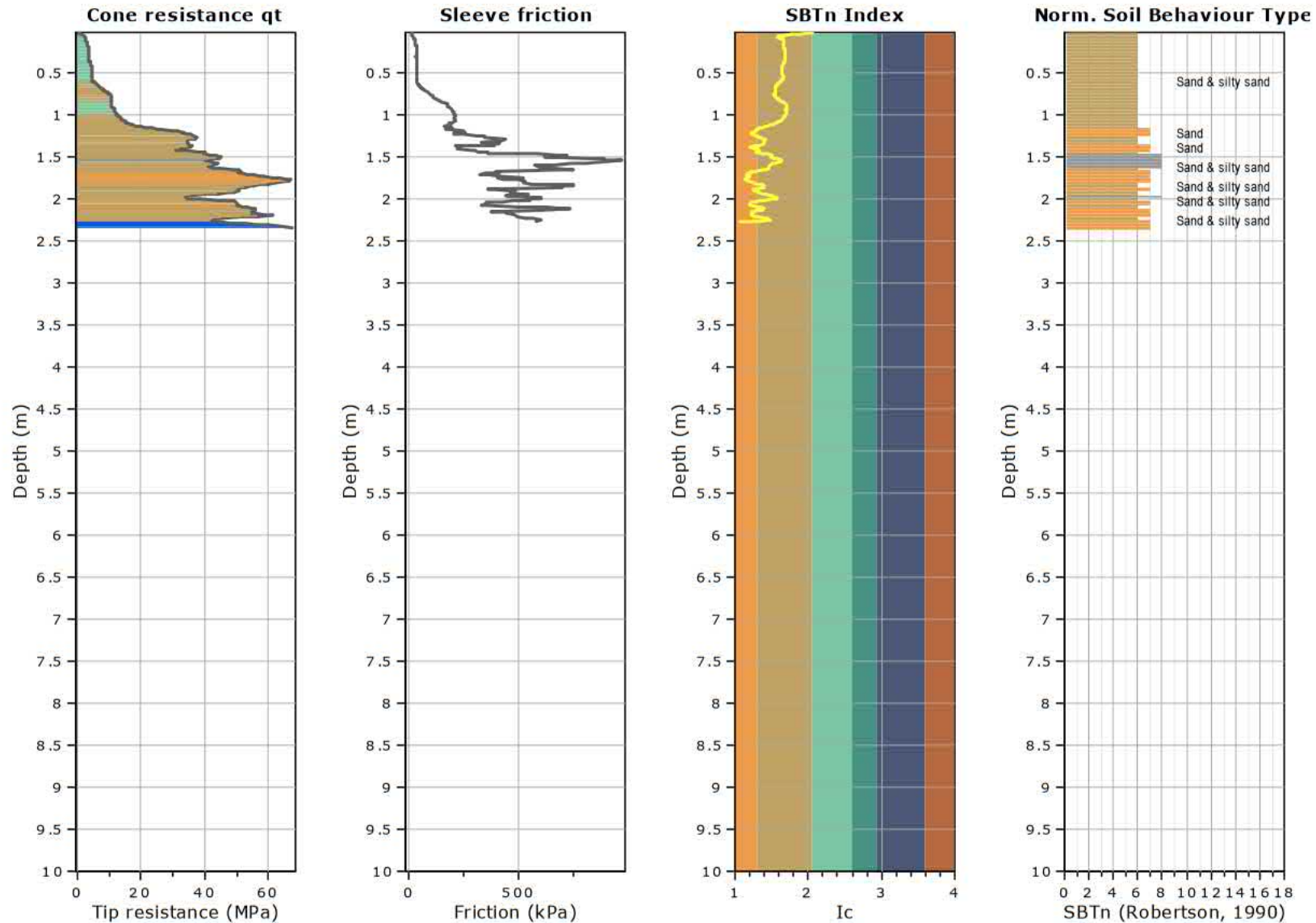


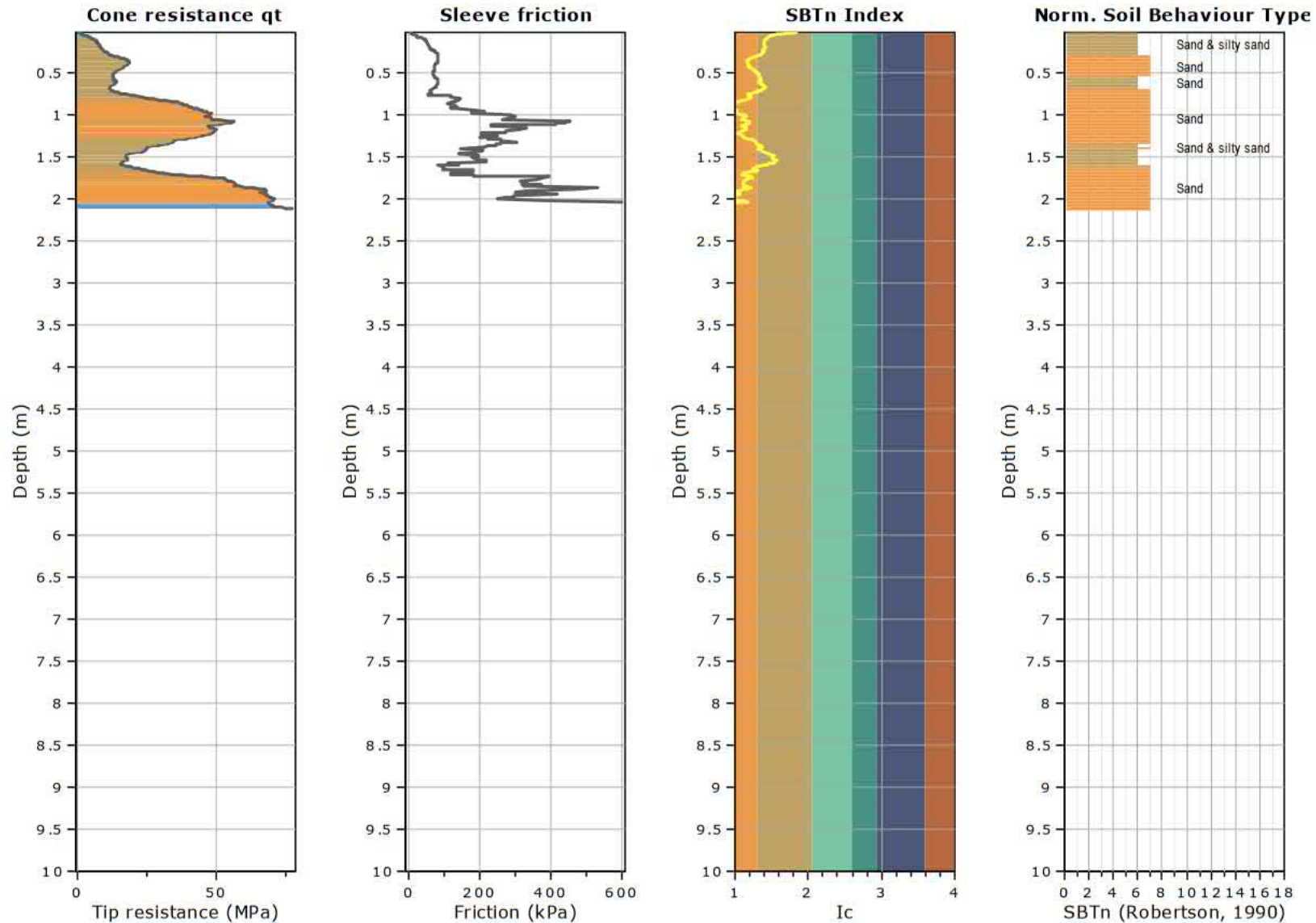


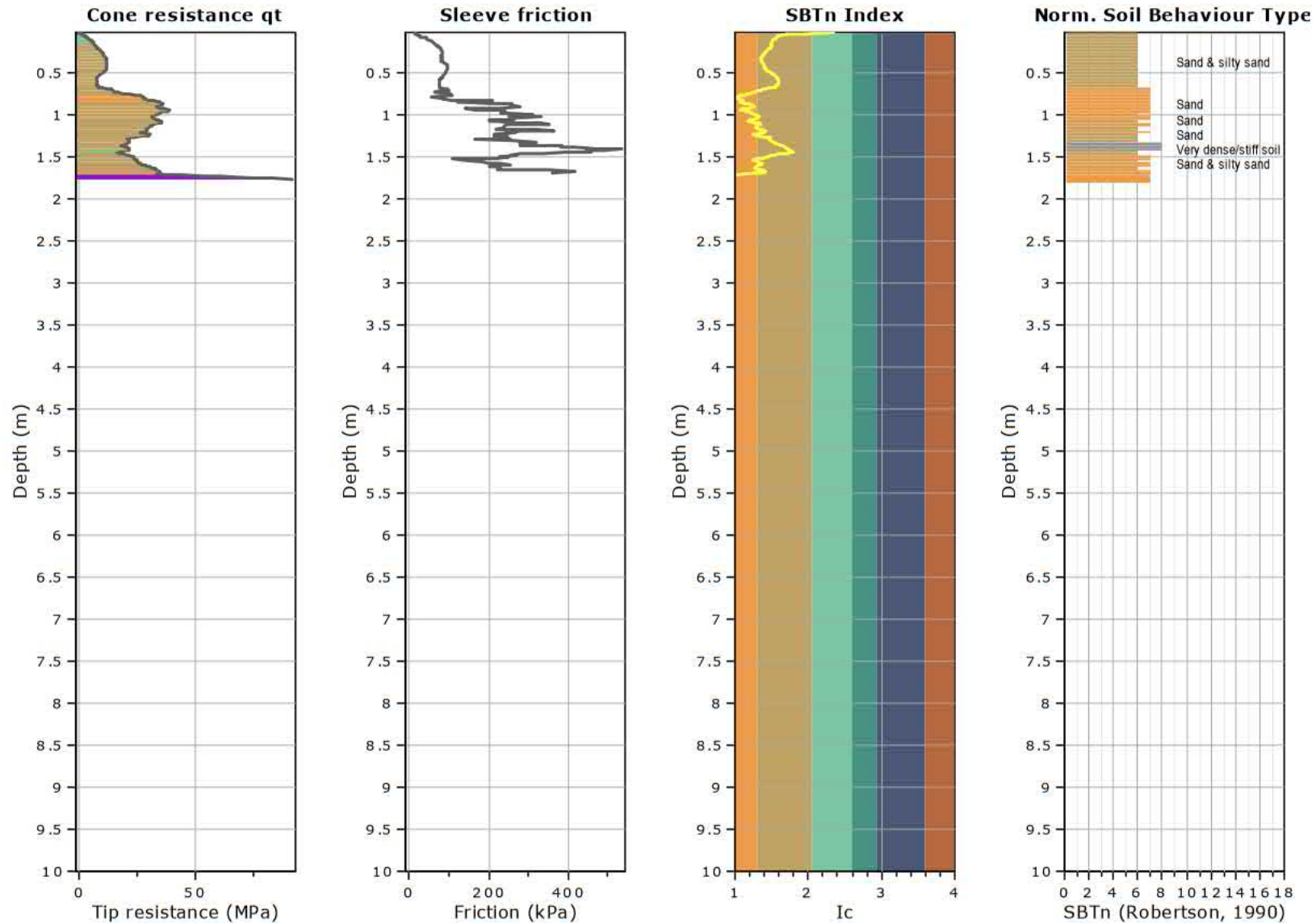


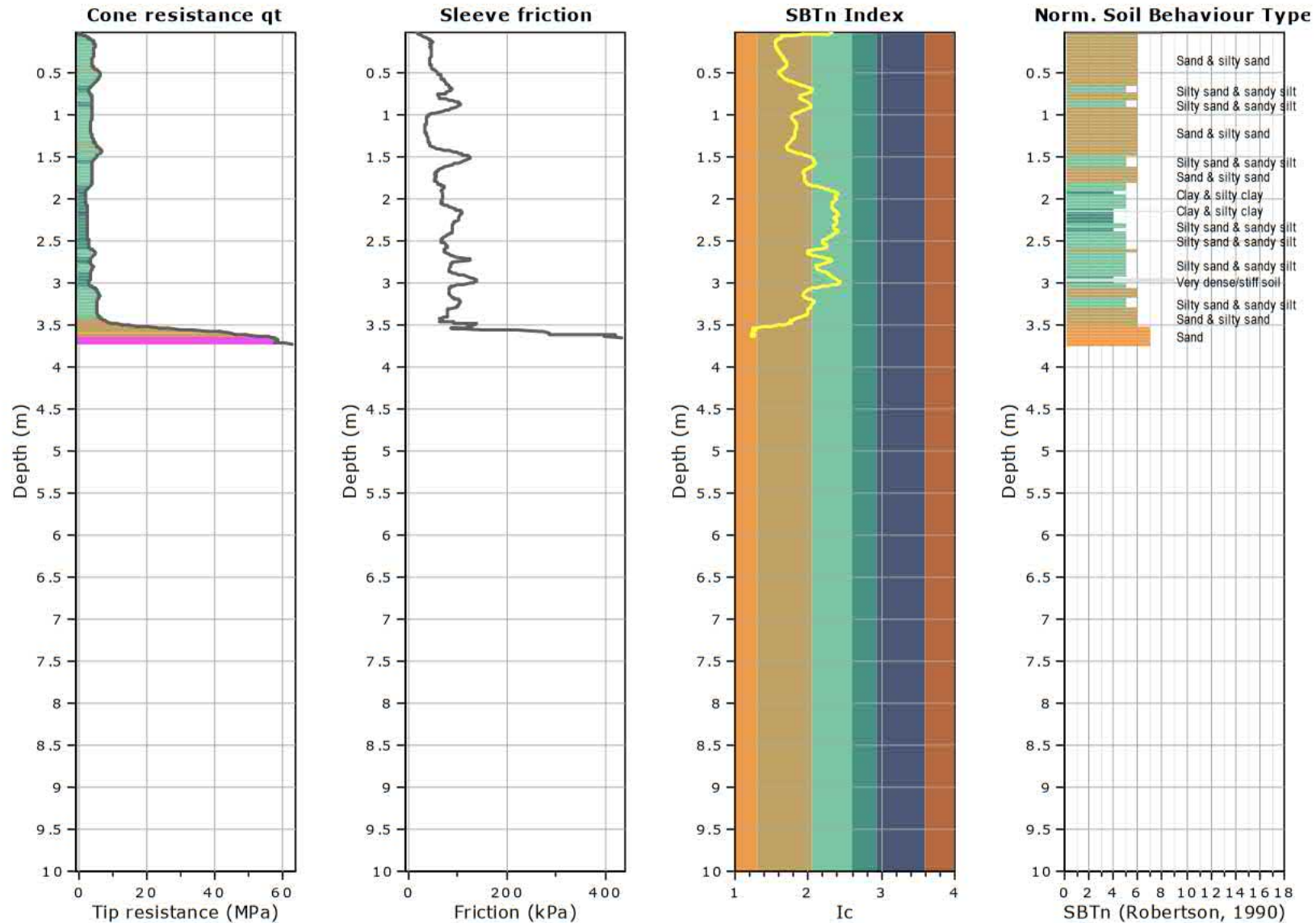


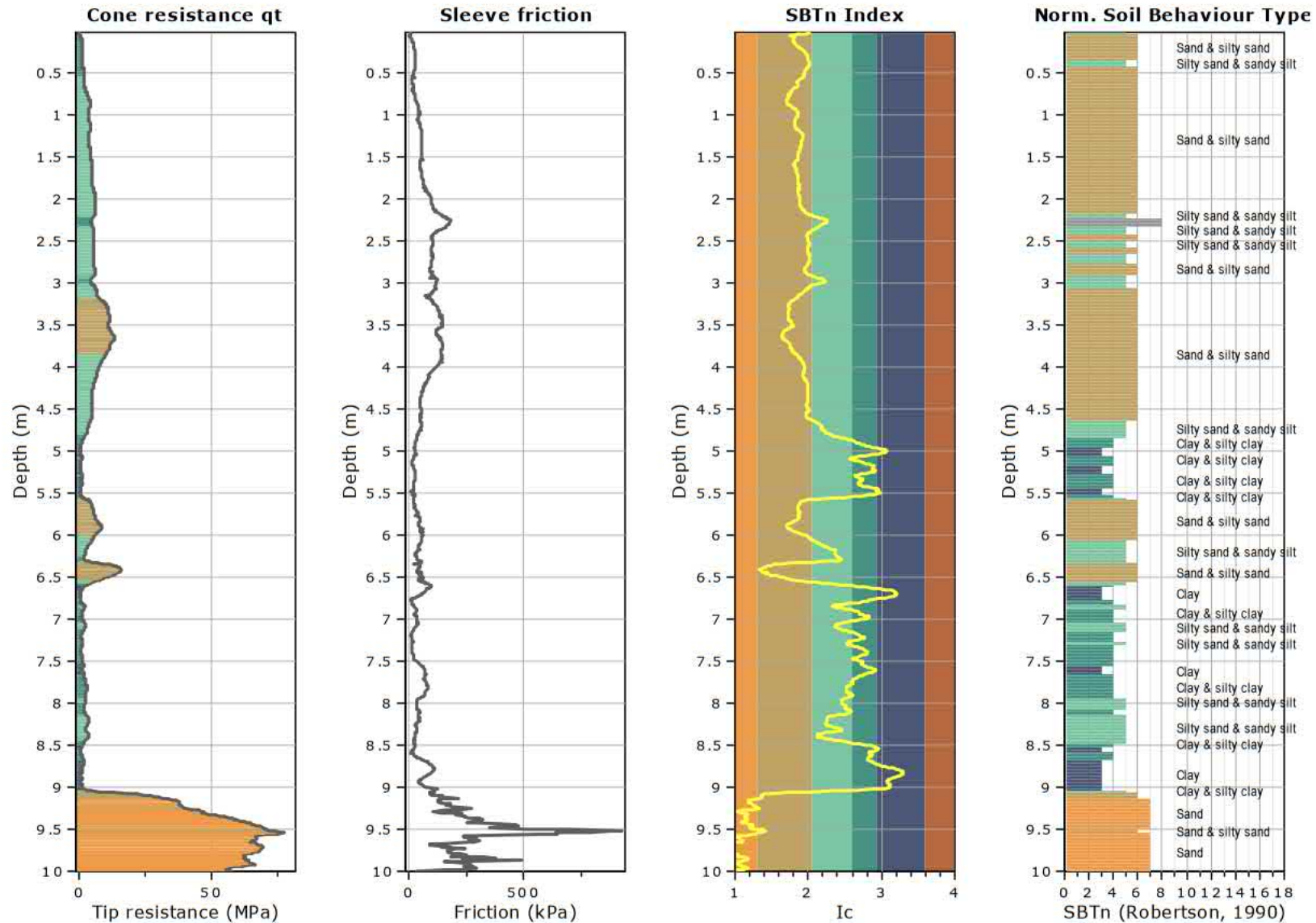


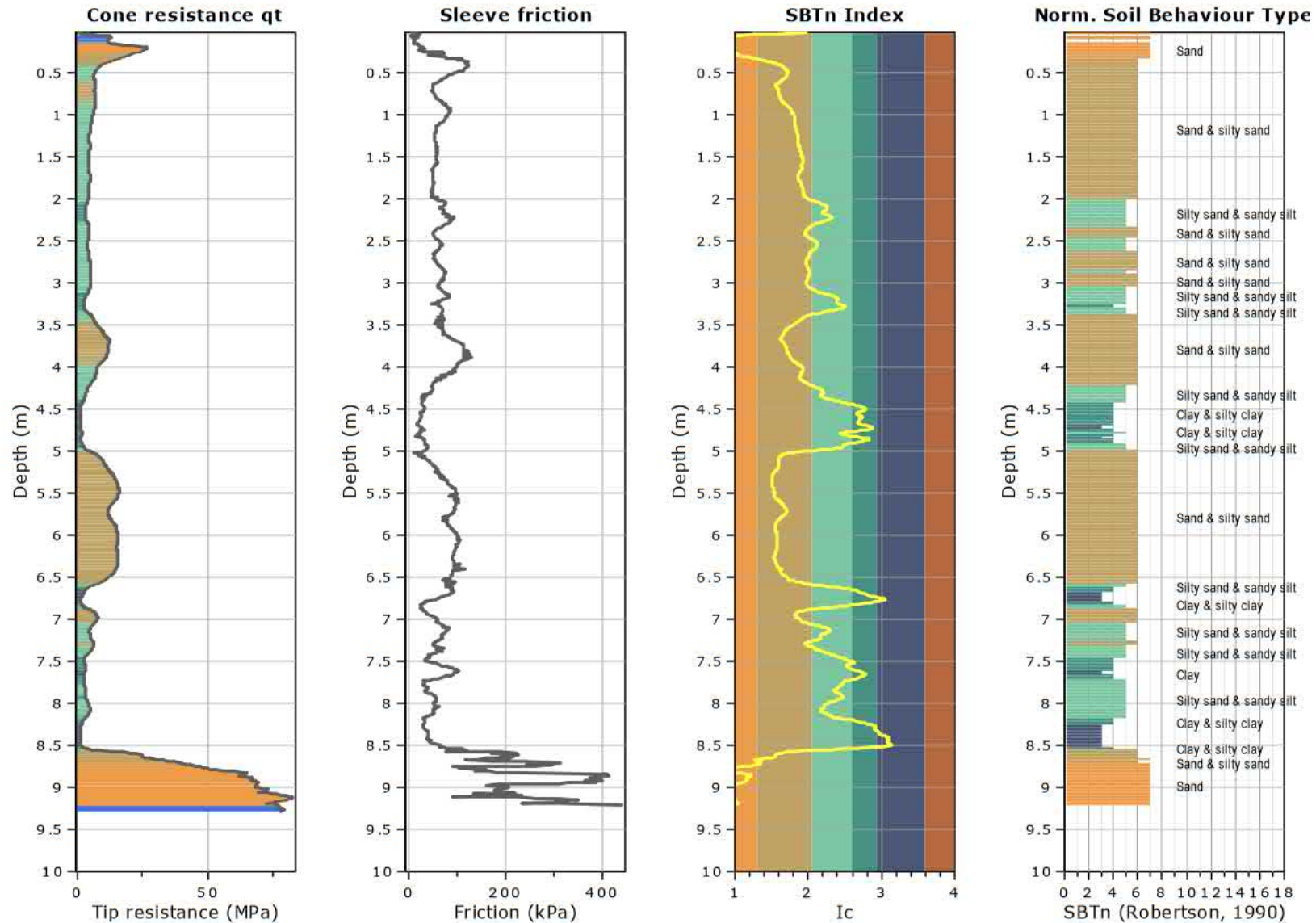














Engineering Log - Borehole

client: **IAG Insurance**

principal: -

project: **IAG Insurance Claims**location: **176 Birchs Road, Prebbleton**Borehole ID: **BH1**



sheet: 1 of 3

project no. **GENZCHRI15217AJR**date started: **17 Oct 2013**date completed: **17 Oct 2013**logged by: **S. Fellers**checked by: **D. Harris**

position: Not Specified surface elevation: Not Specified angle from horizontal: 90°
 drill model: Comacchio MC 900 mounting: Track hole diameter: 100 mm

drilling information					material substance							
method & support	penetration	water	samples & field tests	RL (m)	depth (m)	graph c log	classification symbol	material description SOIL TYPE: plasticity or particle characteristic, colour, secondary and minor components	moisture condition	consistency / relative density	shear vane ⊕ remoulded ⊙ peak (kPa)	structure and additional observations
SHQ3 C	1						ML	TOPSOIL: SILT: non plastic liquid limit, dark brown, with minor rootlets and trace of sand.	M			TOPSOIL
	2						ML	SILT: low liquid limit, pale brown, with minor fine grained sand.		F		SPRINGSTON FORMATION
	3						SM	SILTY SAND: fine to medium, pale brown.		L		
				SPT 1, 1, 1, 1, 1, 2 N=5	1.0				W			
				SPT 1, 1, 1, 2, 2, 1 N=6	2.0				S	St		
							ML	Sandy SILT: low liquid limit, pale brown with grey mottling.				
				SPT 2, 3, 3, 3, 3, 4 N=13	3.0							
							ML	SILT: low liquid limit, grey, with minor organics (sticks and wood fragments), trace of fine grained sand.				
							SP	SAND: fine to medium, dark grey.		L / MD		
								at 5.1m: with minor organics (wood fragments). at 5.3m: organics absent				

method	support	samples & field tests	classification symbol & soil description	consistency / relative density
AD auger drilling*	M mud	U## undisturbed sample ##mm diameter	based on New Zealand Geotechnical Society	VS very soft
AS auger screwing*	C casing	D disturbed sample		S soft
RR roller/tricone		B bulk disturbed sample	F firm	
W washbore		E environmental sample	St stiff	
CT cable tool		HP hand penetrometer (kPa)		VSt very stiff
HA hand auger		N standard penetration test (SPT)		H hard
S sonic*		N* SPT - sample recovered		Fb friable
B blank bit		Nc SPT with solid cone		VL very loose
V V bit		VS vane shearpeak/remoulded (uncorrected kPa)		L loose
T TC bit				MD medium dense
* bit shown by suffix				D dense
e.g. AD/T		R refusal		VD very dense

penetration	
water	



Engineering Log - Borehole

client: **IAG Insurance**

principal: -

project: **IAG Insurance Claims**location: **176 Birchs Road, Prebbleton**Borehole ID: **BH1**

sheet: 2 of 3

project no. **GENZCHRI15217AJR**date started: **17 Oct 2013**date completed: **17 Oct 2013**logged by: **S. Fellers**checked by: **D. Harris**

position: Not Specified

surface elevation: Not Specified

angle from horizontal: 90°

drill model: Comacchio MC 900

mounting: Track

hole diameter: 100 mm

drilling information					material substance										
method & support	1 penetration	2 penetration	3 penetration	water	samples & field tests	RL (m)	depth (m)	graph c log	classification symbol	material description SOIL TYPE: plasticity or particle characteristic, colour, secondary and minor components	moisture condition	consistency / relative density		shear vane remoulded peak (kPa)	structure and additional observations
SHQ3 C	1 2 3						9.0 								

method AD auger drilling* AS auger screwing* RR roller/tricone W washbore CT cable tool HA hand auger S sonic* B blank bit V V bit T TC bit * bit shown by suffix e.g. AD/T	support M mud C casing N nil penetration 10-Oct-12 water level on date shown water inflow water outflow	samples & field tests U## undisturbed sample ##mm diameter D disturbed sample B bulk disturbed sample E environmental sample HP hand penetrometer (kPa) N standard penetration test (SPT) N* SPT - sample recovered Nc SPT with solid cone VS vane shearpeak/remoulded (uncorrected kPa) R refusal	classification symbol & soil description based on New Zealand Geotechnical Society	consistency / relative density VS very soft S soft F firm St stiff VSt very stiff H hard Fb friable VL very loose L loose MD medium dense D dense VD very dense
			moisture D dry M moist W wet S saturated	

CDF_0_g_04A./ (LATEST LIBRARY) GLB Log COF BOREHOLE: NONCORED AJR - BH GINTGPJ <<DrawingFile>> 28/10/2013 16:48



Engineering Log - Borehole

client: **IAG Insurance**

principal: -



project: **IAG Insurance Claims**location: **176 Birchs Road, Prebbleton**Borehole ID: **BH1**

sheet: 3 of 3

project no. **GENZCHRI15217AJR**date started: **17 Oct 2013**date completed: **17 Oct 2013**logged by: **S. Fellers**checked by: **D. Harris**

position: Not Specified surface elevation: Not Specified angle from horizontal: 90°
 drill model: Comacchio MC 900 mounting: Track hole diameter: 100 mm

drilling information				material substance					
method & support	penetration	water	samples & field tests	RL (m)	depth (m)	graph c log	classification symbol	material description	moisture condition
	1 2 3							SOIL TYPE: plasticity or particle characteristic, colour, secondary and minor components	
			SPT 10, 13, 15, 13, 16, 8/35mm N=R		17.0		GW	GRAVEL: fine to coarse, rounded to sub-rounded, with minor sand, trace of cobbles. <i>(continued)</i>	S
					18.0			at 17.6m: with minor silt.	
			SPT 6, 8, 9, 6, 5, 8 N=28		19.0		GP	Sandy GRAVEL: fine to coarse, rounded to sub-angular, sand is fine to coarse grained.	
			SPT 14, 26/65mm N=R		20.0			Borehole BH1 terminated at 19.95 m Target depth	VD
					21.0				
					22.0				
					23.0				

method AD auger drilling* AS auger screwing* RR roller/tricone W washbore CT cable tool HA hand auger S sonic* B blank bit V V bit T TC bit * bit shown by suffix e.g. AD/T	support M mud C casing N nil penetration  no resistance ranging to refusal water  10-Oct-12 water level on date shown water inflow water outflow	samples & field tests U## undisturbed sample ##mm diameter D disturbed sample B bulk disturbed sample E environmental sample HP hand penetrometer (kPa) N standard penetration test (SPT) N* SPT - sample recovered Nc SPT with solid cone VS vane shearpeak/remoulded (uncorrected kPa) R refusal	classification symbol & soil description based on New Zealand Geotechnical Society moisture D dry M moist W wet S saturated	consistency / relative density VS very soft S soft F firm St stiff VSt very stiff H hard Fb friable VL very loose L loose MD medium dense D dense VD very dense
--	--	---	---	--

Notes & Abbreviations

Water

▼ Standing Water Level

▽ Water Level At Time Of Drilling

◁ Out Flow ▷ In Flow

Other Comments



HAND AUGER AND SCALA LOG					Job No.:	171064															
Client: Ryan Geddes Project: Future Site Development Location: 212a Birchs Road, Prebbleton Coordinates: E 1559984.4, N 5172262.4					Hole No.:	HA07/SP07															
					Date:	13/11/2017															
					Logged By:	HH															
					Sheet:	2G															
Subsurface Conditions	Depth (m)	Groundwater	Geological Unit	Graphic Log	Scala Penetrometer (blows / 50mm)																Vane Shear Strength (refer notes for details)
SILT with trace gravel; light brown; dry; Low plasticity Very friable Gravel is fine to medium, subrounded.			TOPSOIL		0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	
SILT with minor sand; light brown; dry; poorly graded Sand is fine to medium.																					

NZGD ID: HADCP110226

Notes & Abbreviations

Water

▼ Standing Water Level
▽ Water Level At Time Of Drilling
◁ Out Flow ▷ In Flow

Other Comments



NZGD ID: HADCP110226

Notes & Abbreviations

Water

▼ Standing Water Level
▽ Water Level At Time Of Drilling
◁ Out Flow ▷ In Flow

Other Comments



Notes & Abbreviations

Water

▼ Standing Water Level
▽ Water Level At Time Of Drilling
◁ Out Flow ▷ In Flow

Other Comments



Notes & Abbreviations

Water

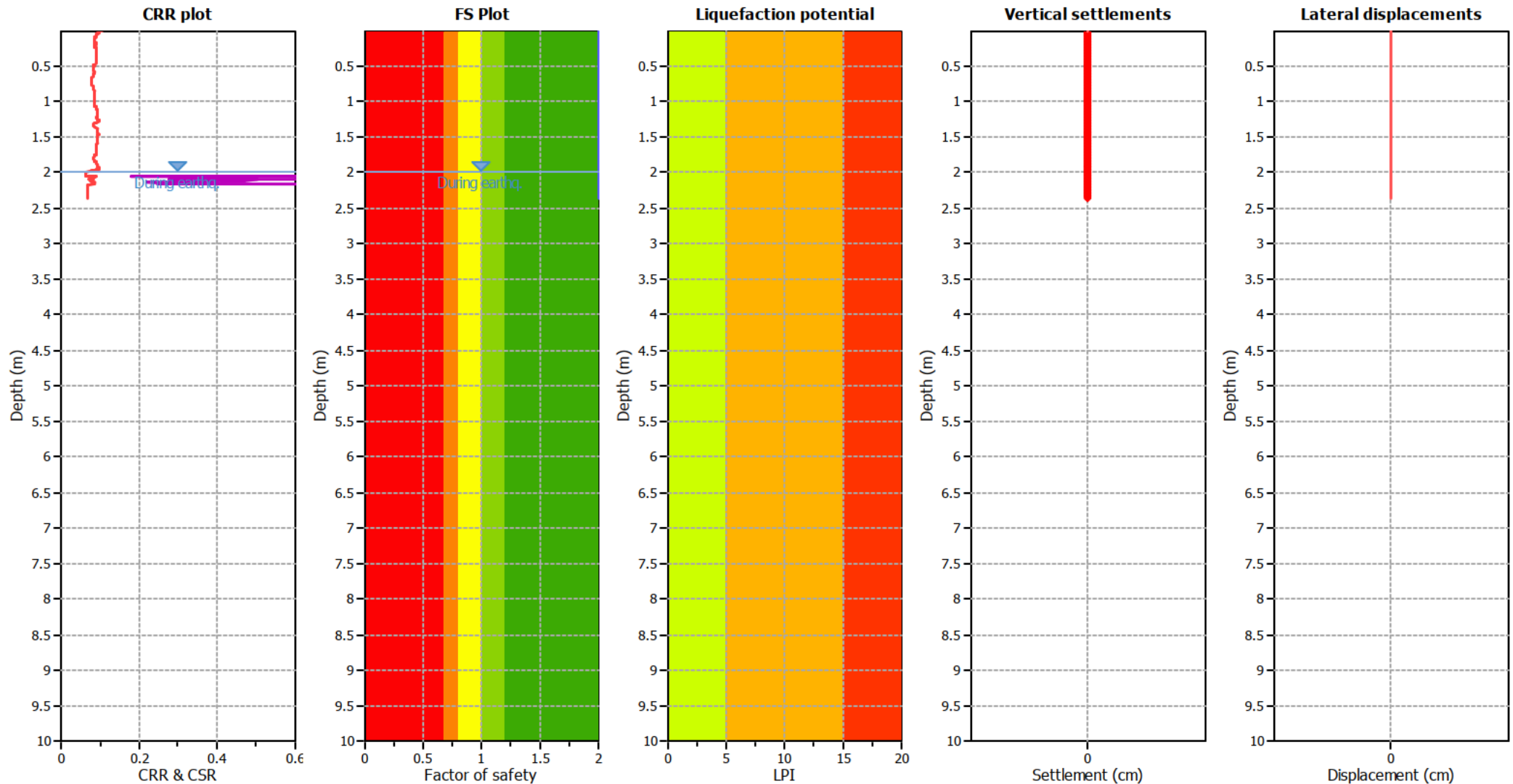
▼ Standing Water Level
▽ Water Level At Time Of Drilling
◁ Out Flow ▷ In Flow

Other Comments



Appendix B – Liquefaction analysis

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	6.00	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.19	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	2.00 m	Fill height:	N/A	Limit depth:	10.00 m

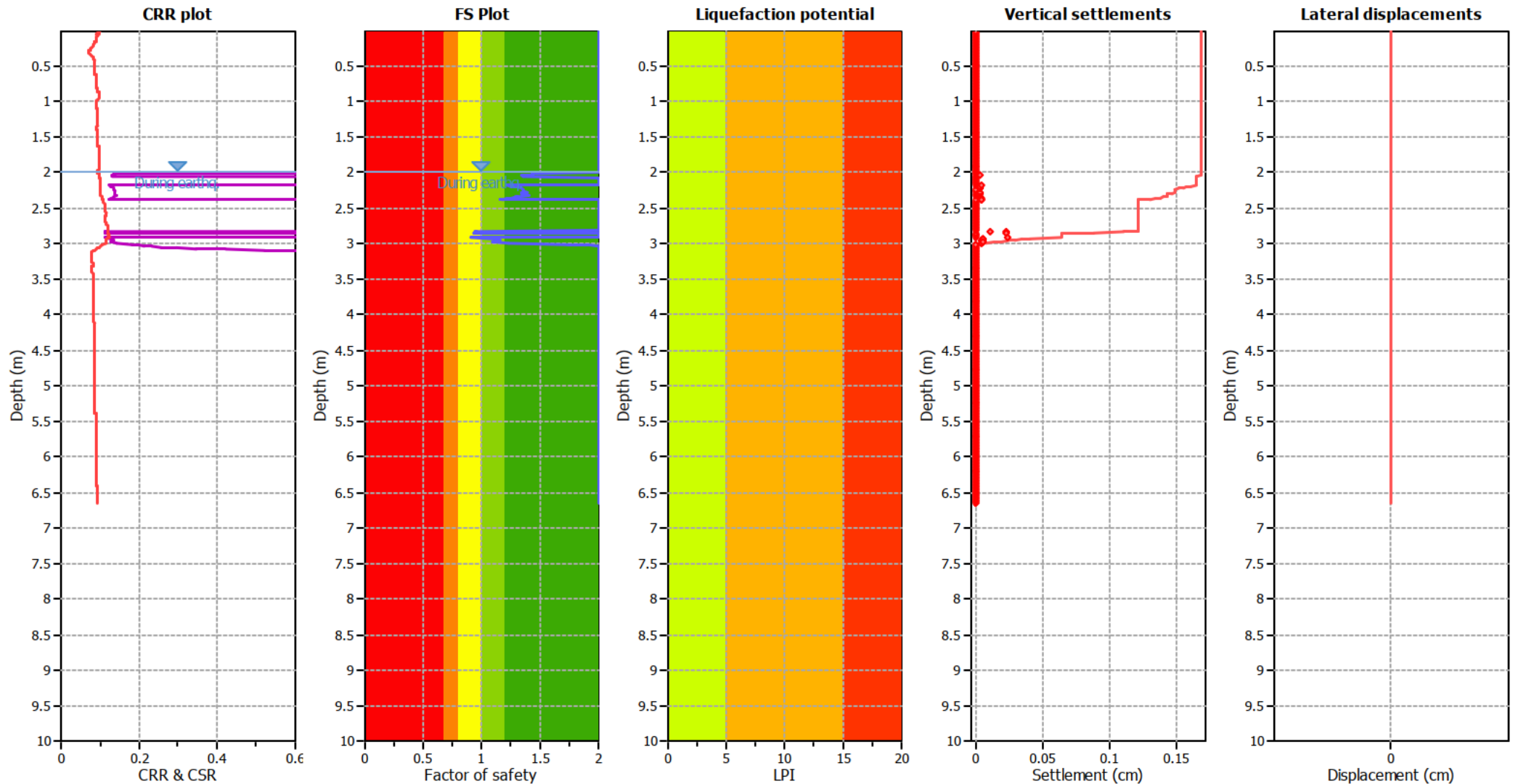
F.S. color scheme

■	Almost certain it will liquefy
■	Very likely to liquefy
■	Liquefaction and no liq. are equally likely
■	Unlike to liquefy
■	Almost certain it will not liquefy

LPI color scheme

■	Very high risk
■	High risk
■	Low risk

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (earthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_s applied:	Yes
Earthquake magnitude M_w :	6.00	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.19	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	2.00 m	Fill height:	N/A	Limit depth:	10.00 m

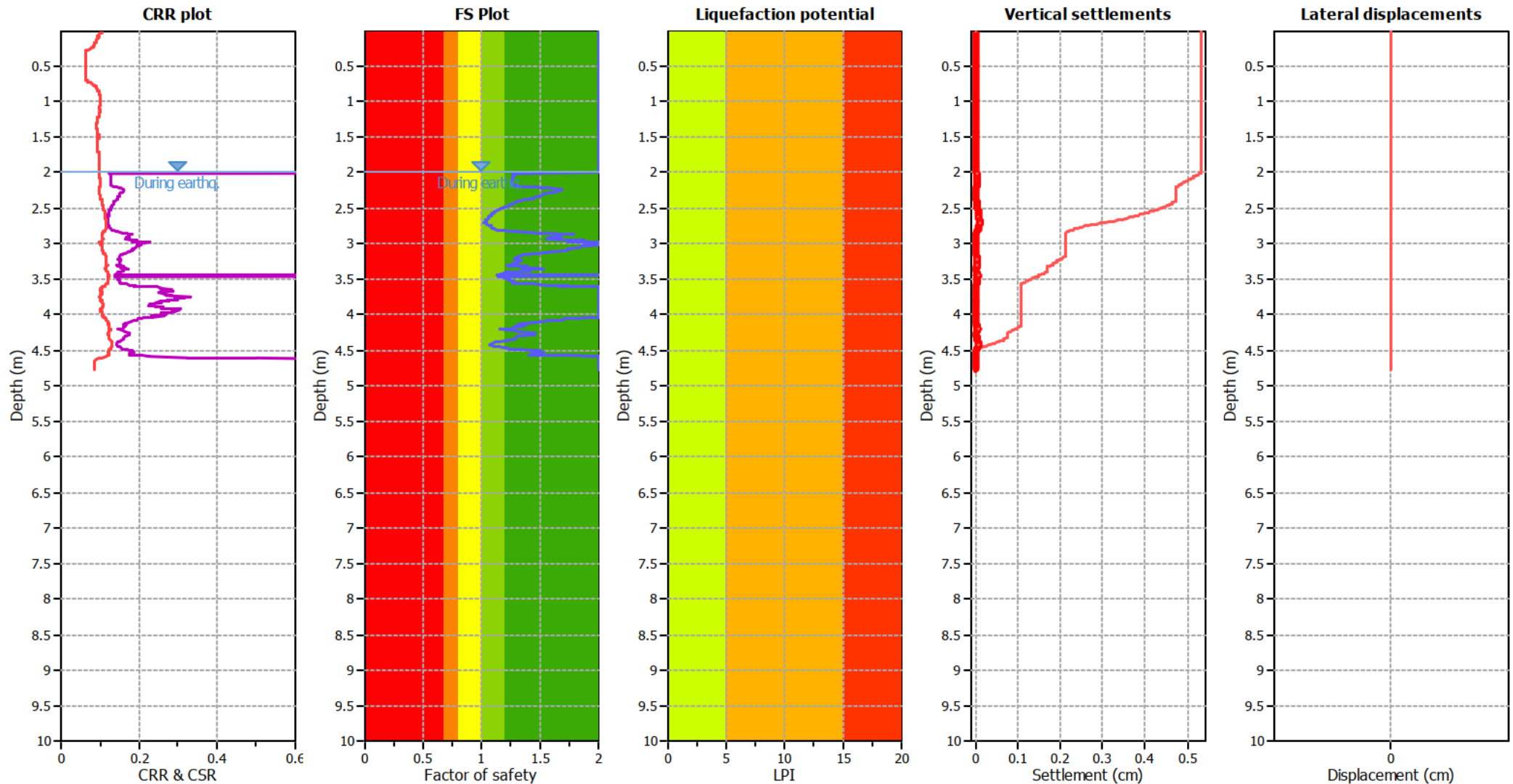
F.S. color scheme

Red	Almost certain it will liquefy
Orange	Very likely to liquefy
Yellow	Liquefaction and no liq. are equally likely
Green	Unlike to liquefy
Dark Green	Almost certain it will not liquefy

LPI color scheme

Red	Very high risk
Orange	High risk
Yellow	Low risk

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (earthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_0 applied:	Yes
Earthquake magnitude M_w :	6.00	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.19	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	2.00 m	Fill height:	N/A	Limit depth:	10.00 m

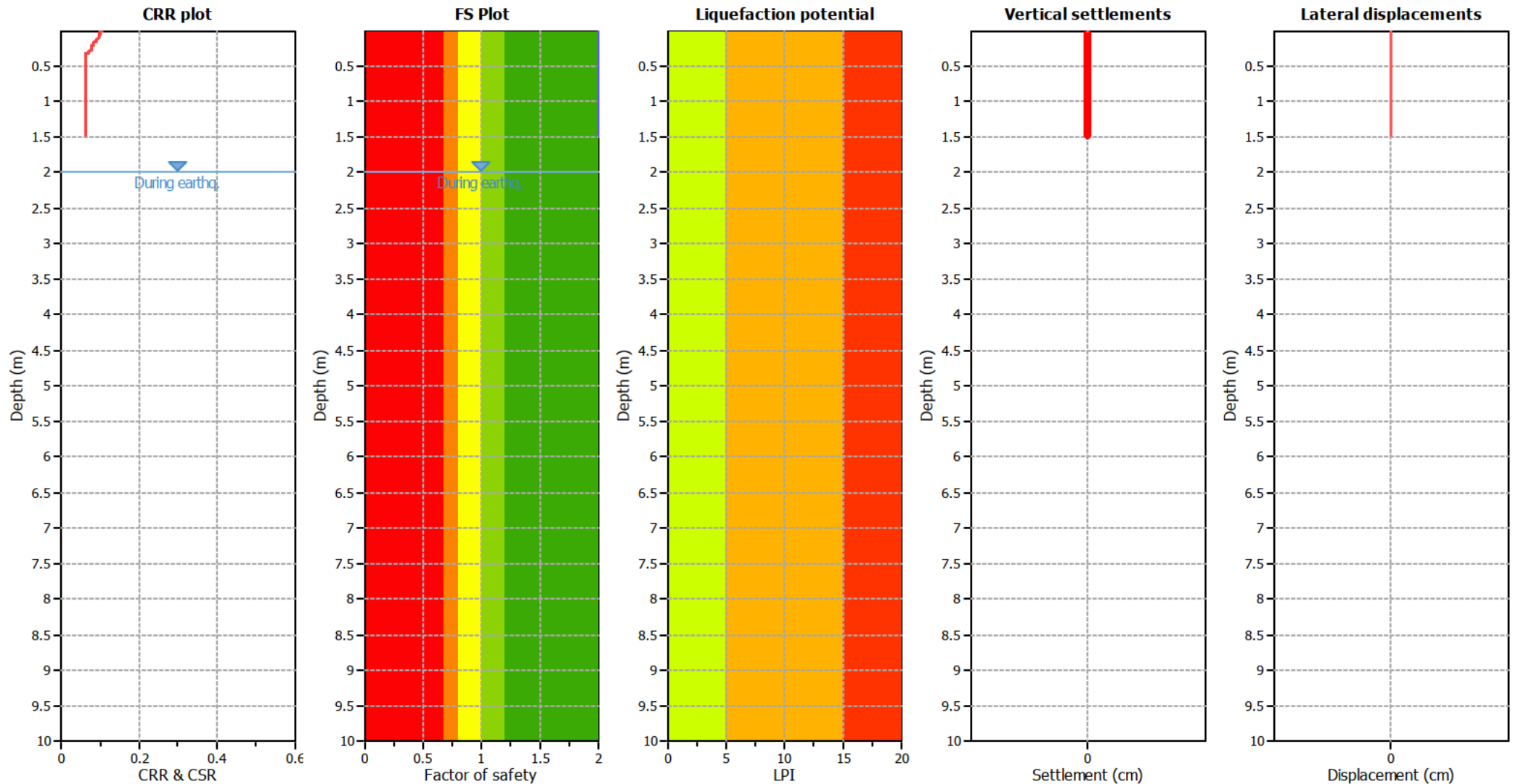
F.S. color scheme

■	Almost certain it will liquefy
■	Very likely to liquefy
■	Liquefaction and no liq. are equally likely
■	Unlike to liquefy
■	Almost certain it will not liquefy

LPI color scheme

■	Very high risk
■	High risk
■	Low risk

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method: B&I (2014)
 Fines correction method: B&I (2014)
 Points to test: Based on Ic value
 Earthquake magnitude M_w : 6.00
 Peak ground acceleration: 0.19
 Depth to water table (insitu): 2.00 m

Depth to GWT (earthq.): 2.00 m
 Average results interval: 3
 Ic cut-off value: 2.60
 Unit weight calculation: Based on SBT
 Use fill: No
 Fill height: N/A

Fill weight: N/A
 Transition detect. applied: No
 K_{σ} applied: Yes
 Clay like behavior applied: Sands only
 Limit depth applied: Yes
 Limit depth: 10.00 m

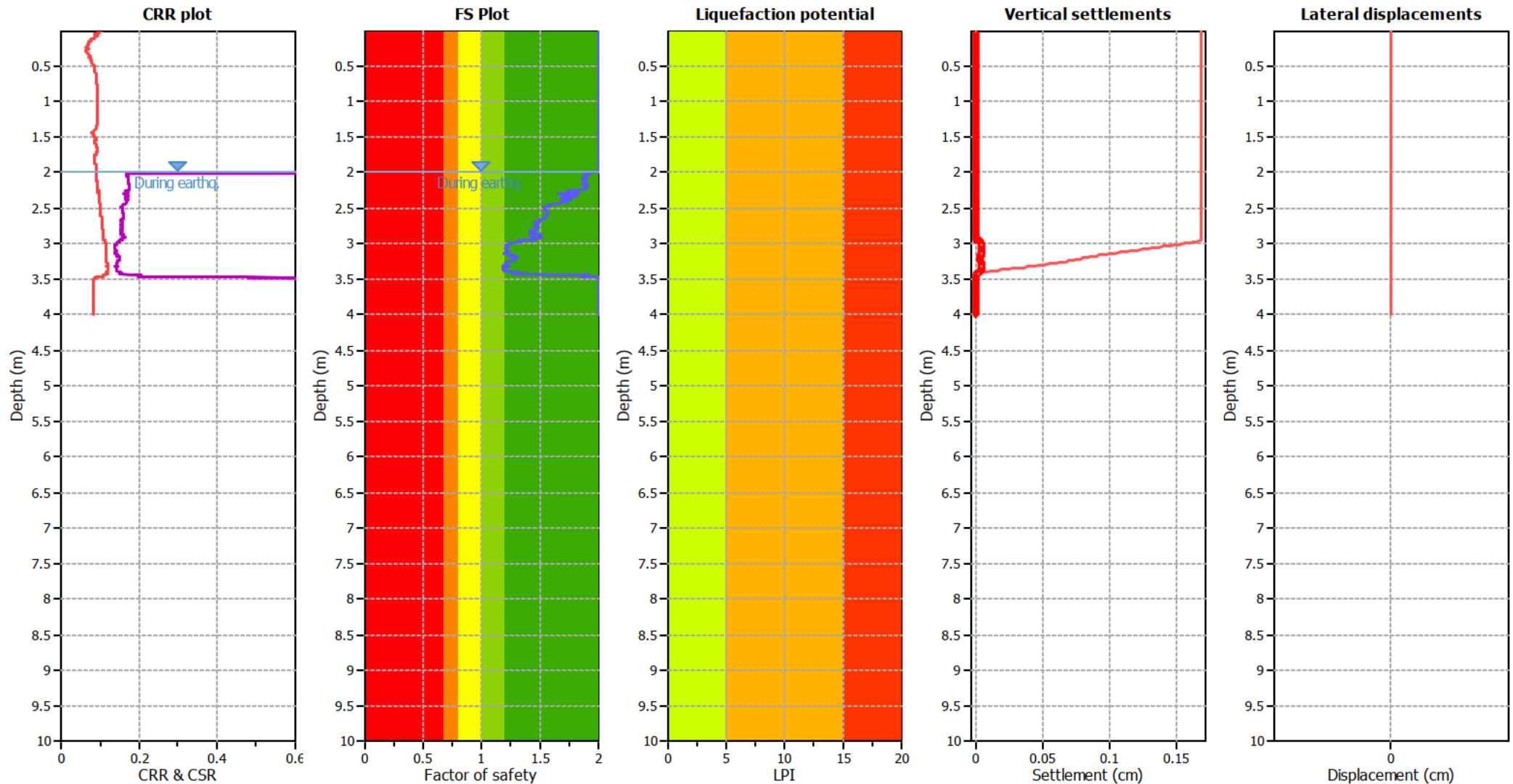
F.S. color scheme

■ Almost certain it will liquefy
■ Very likely to liquefy
■ Liquefaction and no liq. are equally likely
■ Unlike to liquefy
■ Almost certain it will not liquefy

LPI color scheme

■ Very high risk
■ High risk
■ Low risk

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (earthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_s applied:	Yes
Earthquake magnitude M_w :	6.00	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.19	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	2.00 m	Fill height:	N/A	Limit depth:	10.00 m

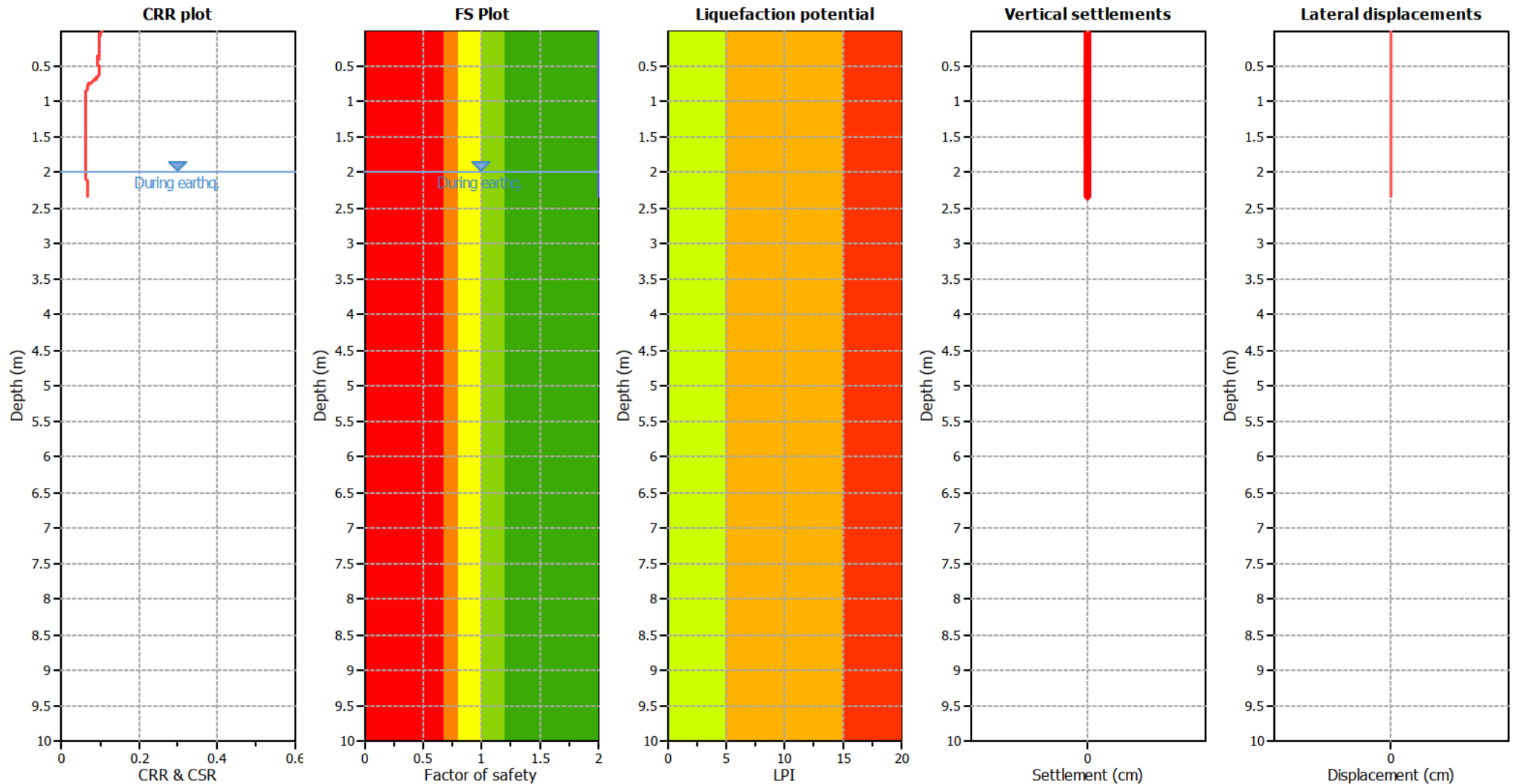
F.S. color scheme

■	Almost certain it will liquefy
■	Very likely to liquefy
■	Liquefaction and no liq. are equally likely
■	Unlike to liquefy
■	Almost certain it will not liquefy

LPI color scheme

■	Very high risk
■	High risk
■	Low risk

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method: B&I (2014)
 Fines correction method: B&I (2014)
 Points to test: Based on Ic value
 Earthquake magnitude M_w : 6.00
 Peak ground acceleration: 0.19
 Depth to water table (insitu): 2.00 m

Depth to GWT (earthq.): 2.00 m
 Average results interval: 3
 Ic cut-off value: 2.60
 Unit weight calculation: Based on SBT
 Use fill: No
 Fill height: N/A

Fill weight: N/A
 Transition detect. applied: No
 K_0 applied: Yes
 Clay like behavior applied: Sands only
 Limit depth applied: Yes
 Limit depth: 10.00 m

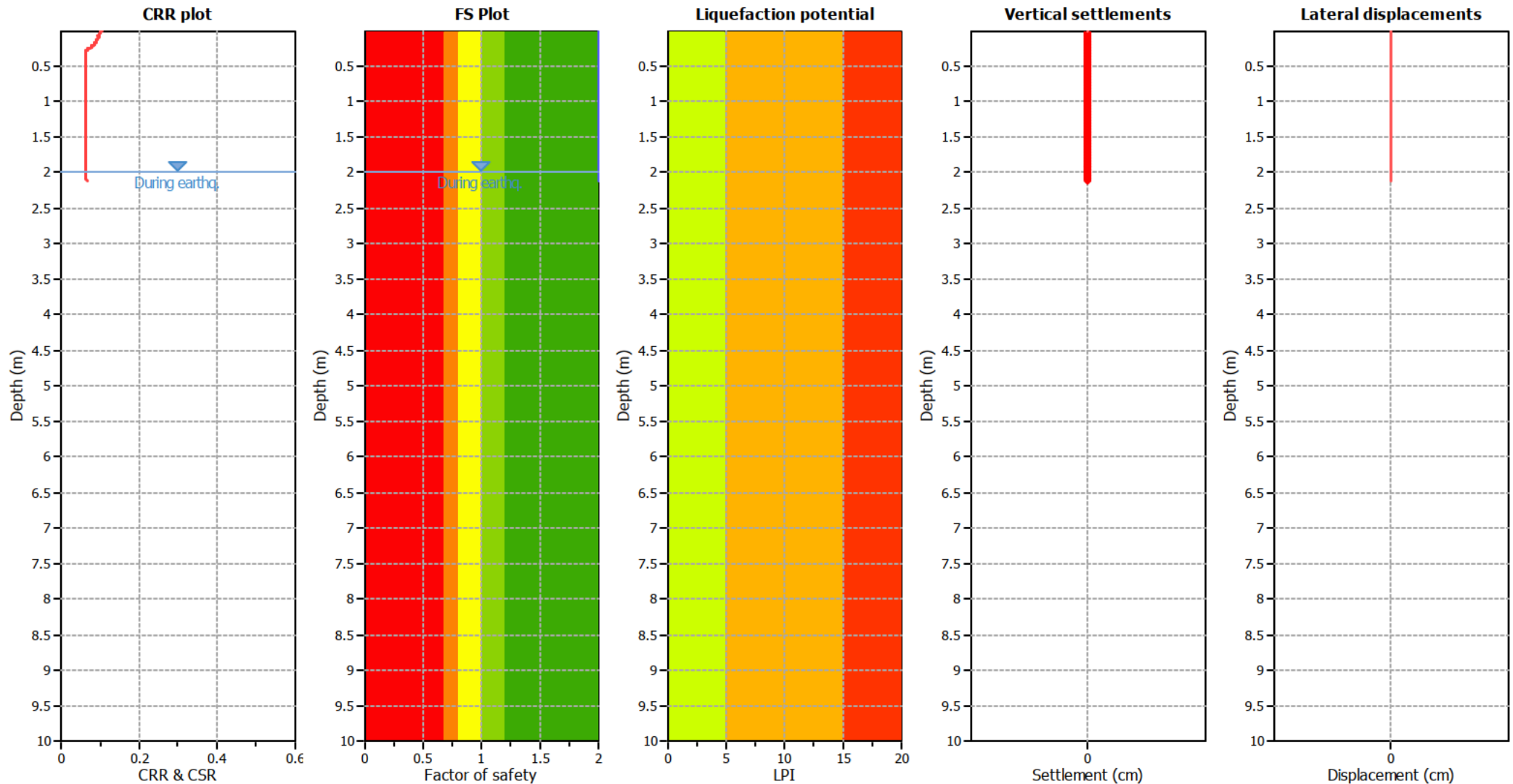
F.S. color scheme

■ Almost certain it will liquefy
■ Very likely to liquefy
■ Liquefaction and no liq. are equally likely
■ Unlike to liquefy
■ Almost certain it will not liquefy

LPI color scheme

■ Very high risk
■ High risk
■ Low risk

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method: B&I (2014)
 Fines correction method: B&I (2014)
 Points to test: Based on I_c value
 Earthquake magnitude M_w : 6.00
 Peak ground acceleration: 0.19
 Depth to water table (insitu): 2.00 m

Depth to GWT (earthq.): 2.00 m
 Average results interval: 3
 I_c cut-off value: 2.60
 Unit weight calculation: Based on SBT
 Use fill: No
 Fill height: N/A

Fill weight: N/A
 Transition detect. applied: No
 K_{σ} applied: Yes
 Clay like behavior applied: Sands only
 Limit depth applied: Yes
 Limit depth: 10.00 m

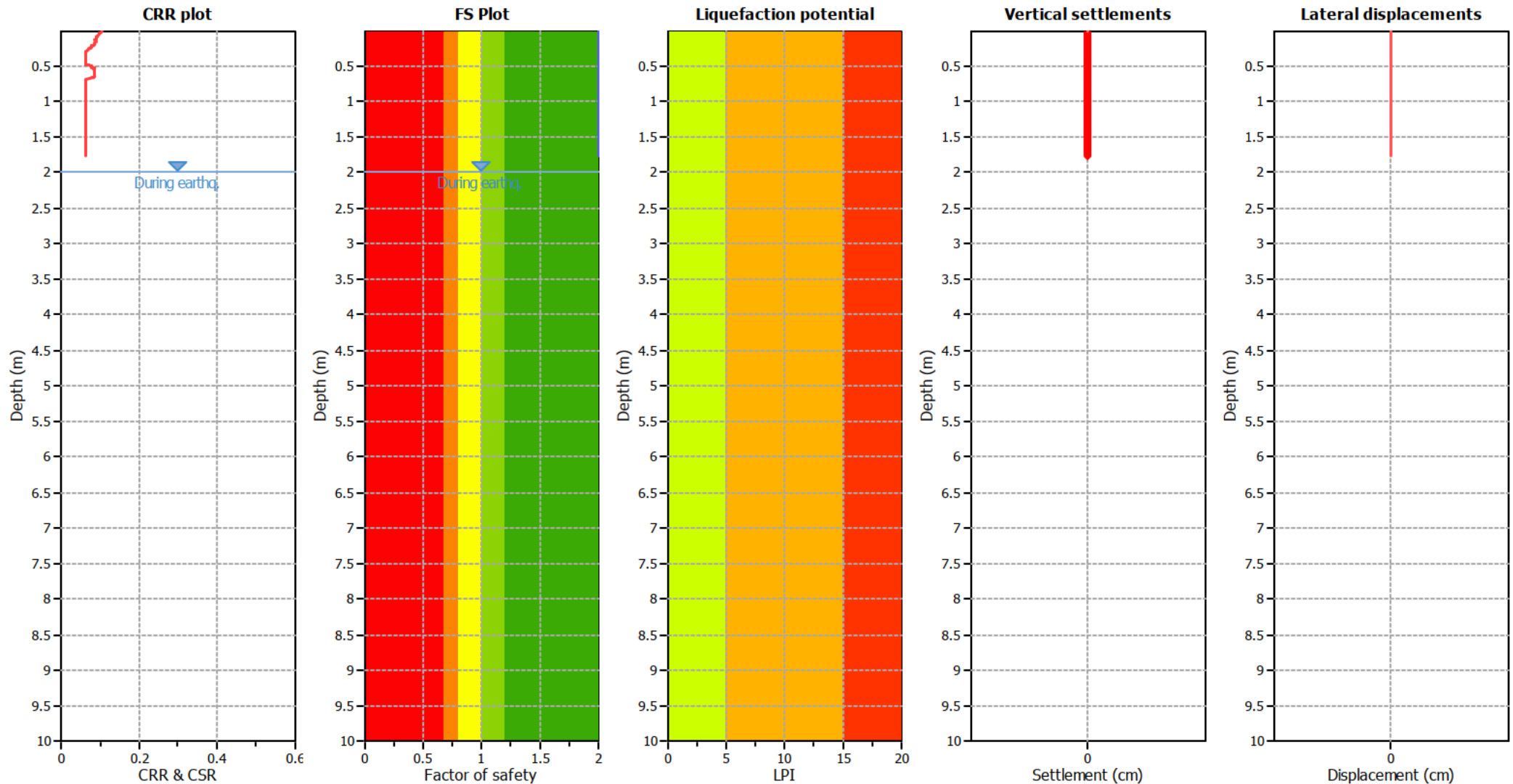
F.S. color scheme

■ Almost certain it will liquefy
■ Very likely to liquefy
■ Liquefaction and no liq. are equally likely
■ Unlike to liquefy
■ Almost certain it will not liquefy

LPI color scheme

■ Very high risk
■ High risk
■ Low risk

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (earthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	6.00	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.19	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	2.00 m	Fill height:	N/A	Limit depth:	10.00 m

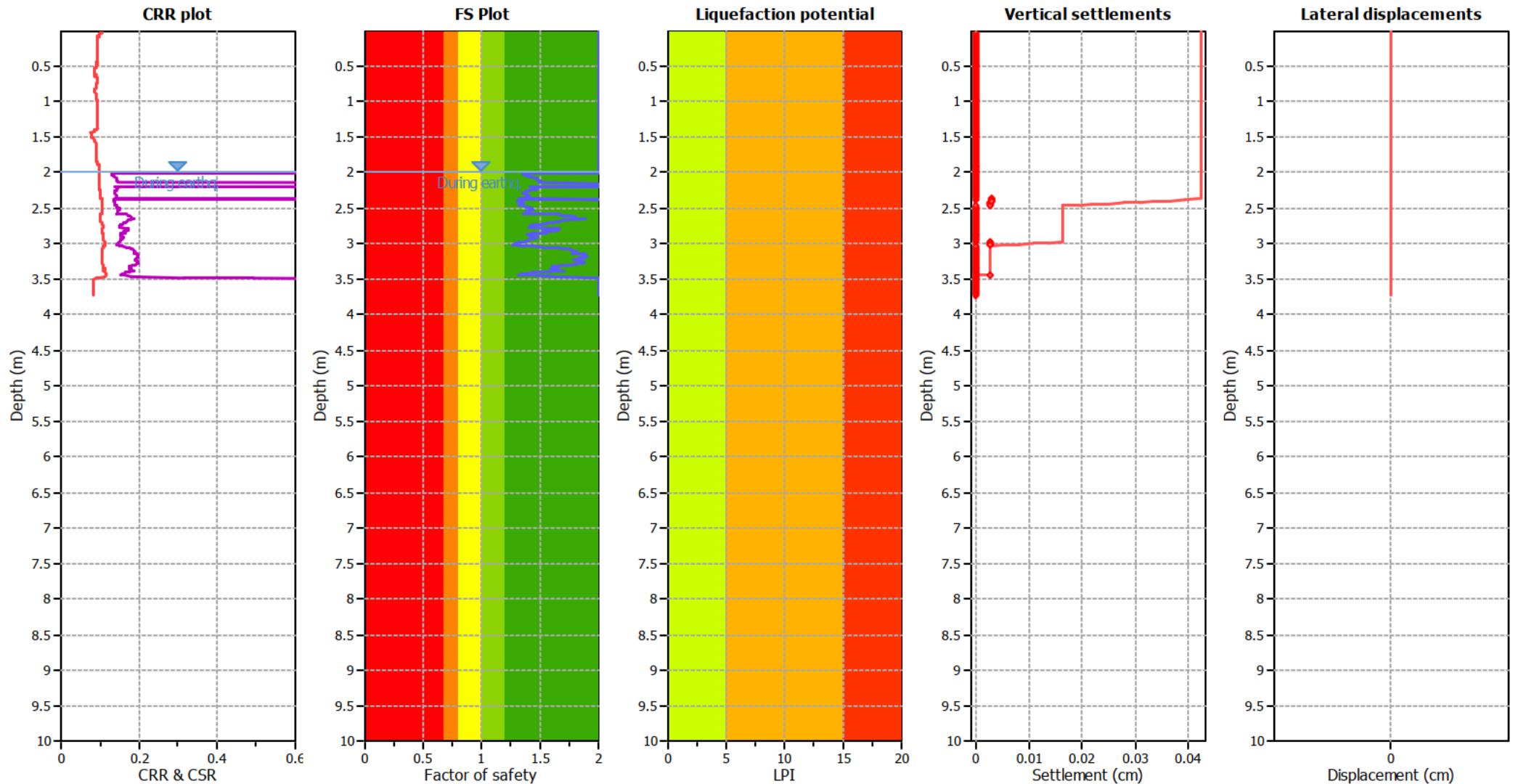
F.S. color scheme

■	Almost certain it will liquefy
■	Very likely to liquefy
■	Liquefaction and no liq. are equally likely
■	Unlike to liquefy
■	Almost certain it will not liquefy

LPI color scheme

■	Very high risk
■	High risk
■	Low risk

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (earthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	6.00	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.19	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	2.00 m	Fill height:	N/A	Limit depth:	10.00 m

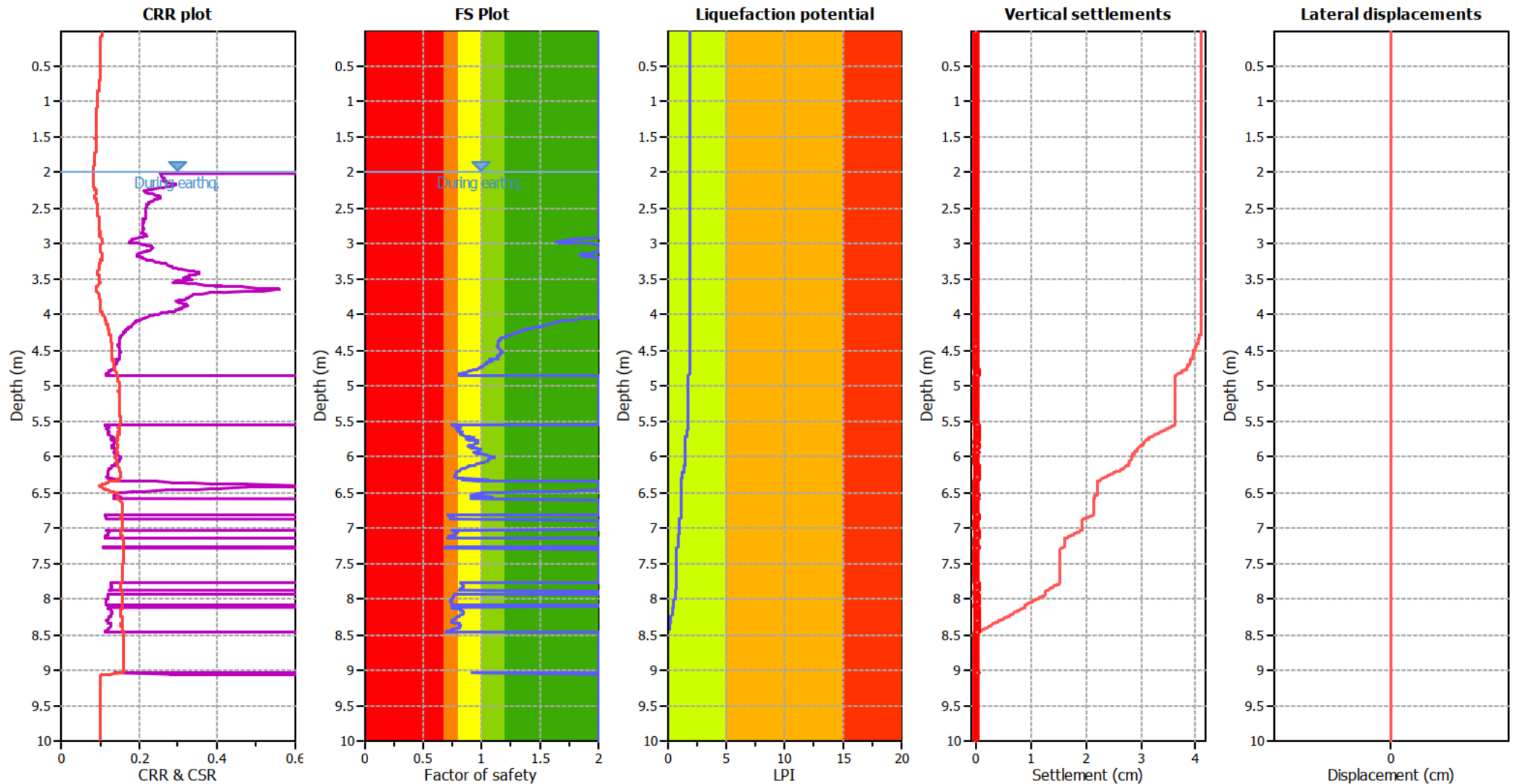
F.S. color scheme

■	Almost certain it will liquefy
■	Very likely to liquefy
■	Liquefaction and no liq. are equally likely
■	Unlike to liquefy
■	Almost certain it will not liquefy

LPI color scheme

■	Very high risk
■	High risk
■	Low risk

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (earthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	6.00	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.19	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	2.00 m	Fill height:	N/A	Limit depth:	10.00 m

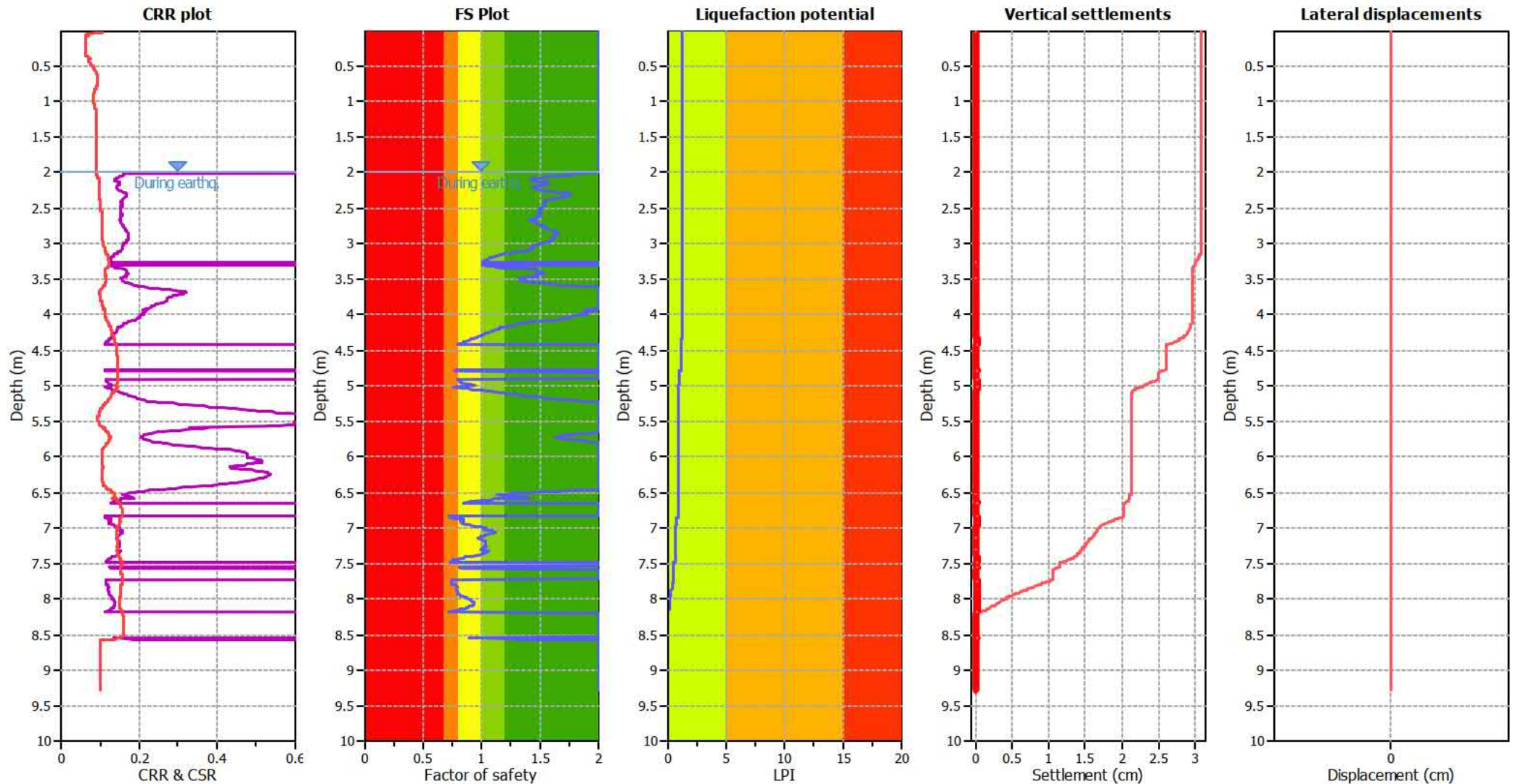
F.S. color scheme

■	Almost certain it will liquefy
■	Very likely to liquefy
■	Liquefaction and no liq. are equally likely
■	Unlike to liquefy
■	Almost certain it will not liquefy

LPI color scheme

■	Very high risk
■	High risk
■	Low risk

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (earthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_s applied:	Yes
Earthquake magnitude M_w :	6.00	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.19	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	2.00 m	Fill height:	N/A	Limit depth:	10.00 m

F.S. color scheme

■	Almost certain it will liquefy
■	Very likely to liquefy
■	Liquefaction and no liq. are equally likely
■	Unlike to liquefy
■	Almost certain it will not liquefy

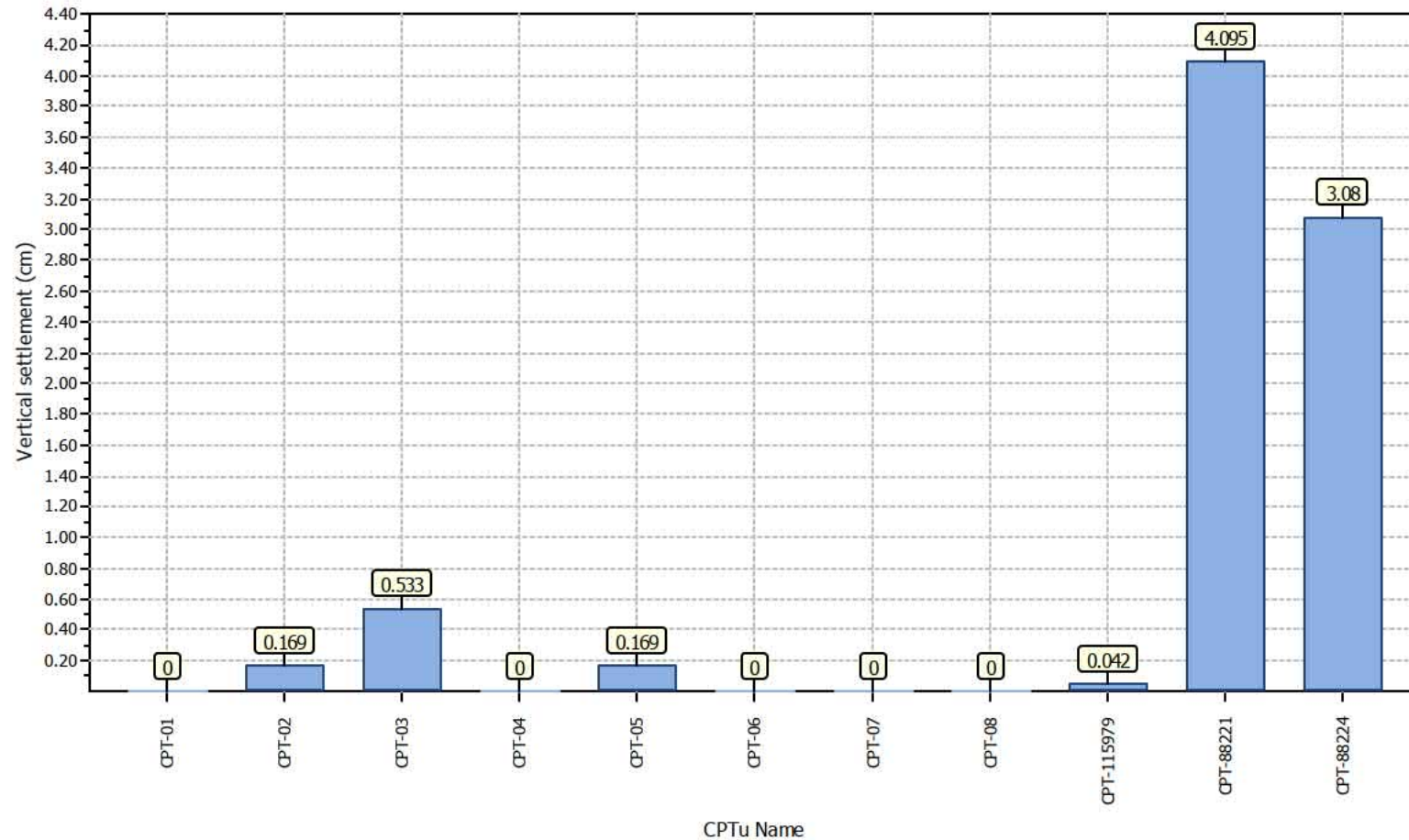
LPI color scheme

■	Very high risk
■	High risk
■	Low risk

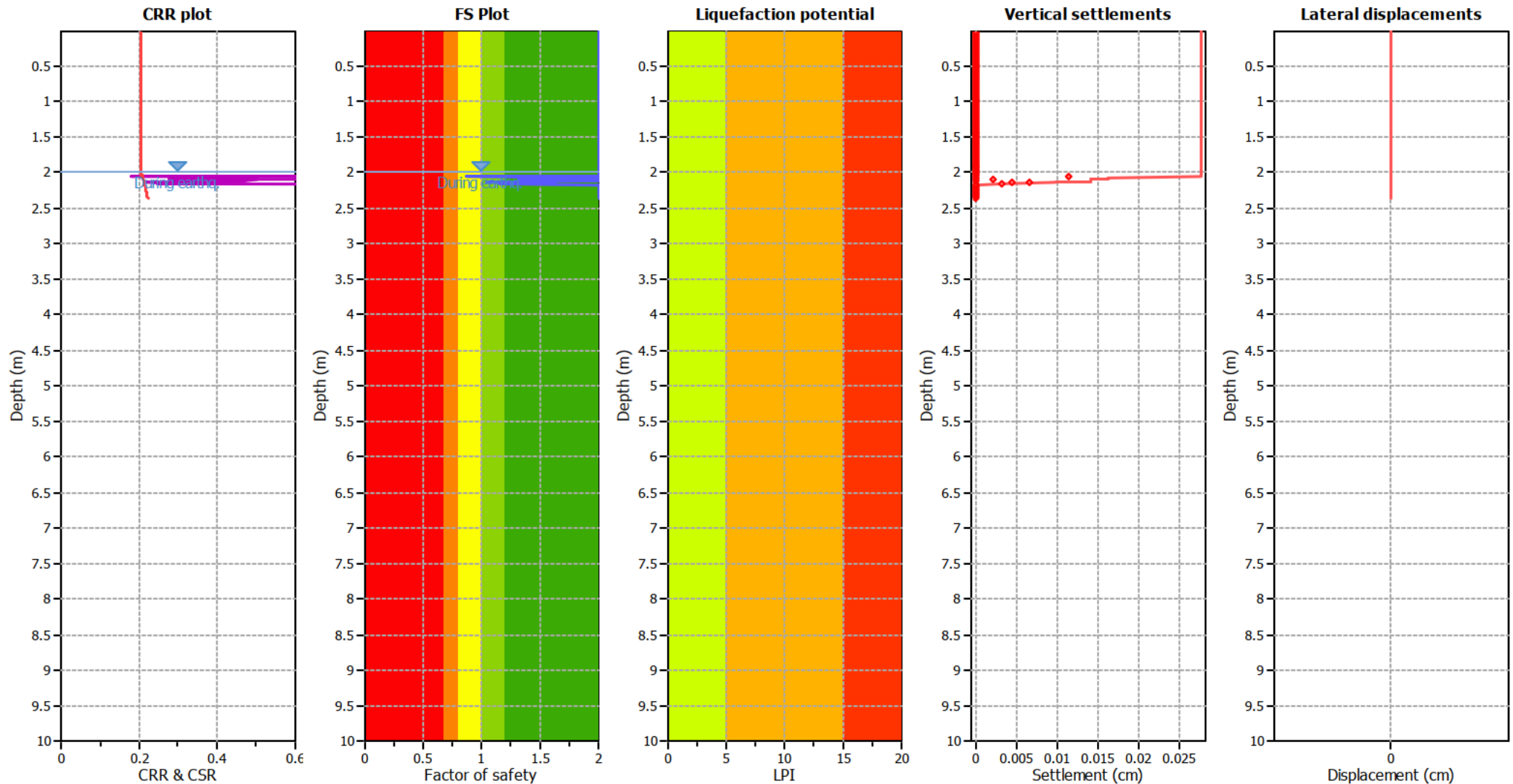
Project title : Birches Village - SLS assessment

Location : Prebbleton, Christchurch

Overall vertical settlements report



Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method: B&I (2014)
 Fines correction method: B&I (2014)
 Points to test: Based on I_c value
 Earthquake magnitude M_w : 7.50
 Peak ground acceleration: 0.35
 Depth to water table (insitu): 2.00 m

Depth to GWT (erthq.): 2.00 m
 Average results interval: 3
 I_c cut-off value: 2.60
 Unit weight calculation: Based on SBT
 Use fill: No
 Fill height: N/A

Fill weight: N/A
 Transition detect. applied: No
 K_{σ} applied: Yes
 Clay like behavior applied: Sands only
 Limit depth applied: Yes
 Limit depth: 10.00 m

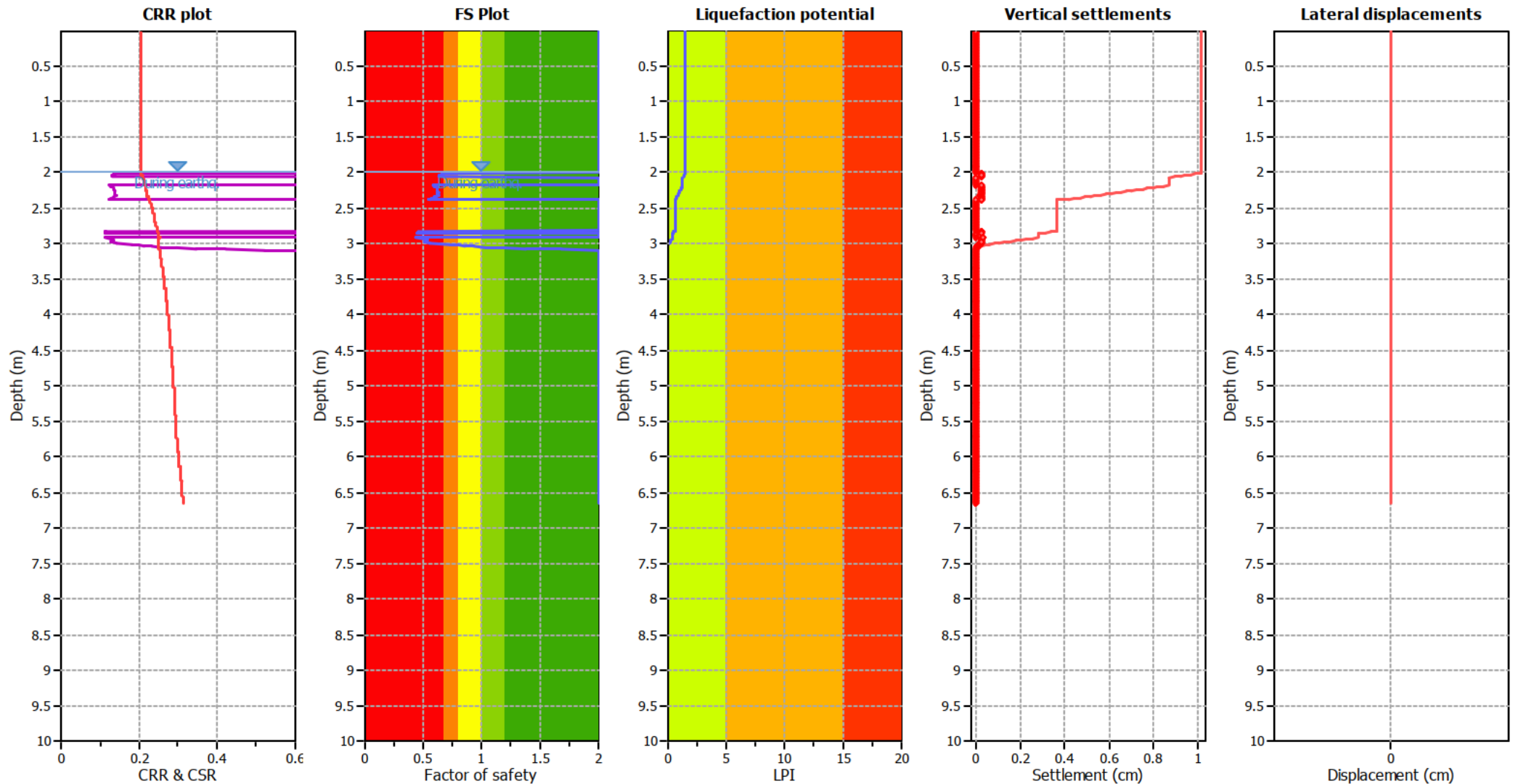
F.S. color scheme

■ Almost certain it will liquefy
■ Very likely to liquefy
■ Liquefaction and no liq. are equally likely
■ Unlike to liquefy
■ Almost certain it will not liquefy

LPI color scheme

■ Very high risk
■ High risk
■ Low risk

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.50	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.35	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	2.00 m	Fill height:	N/A	Limit depth:	10.00 m

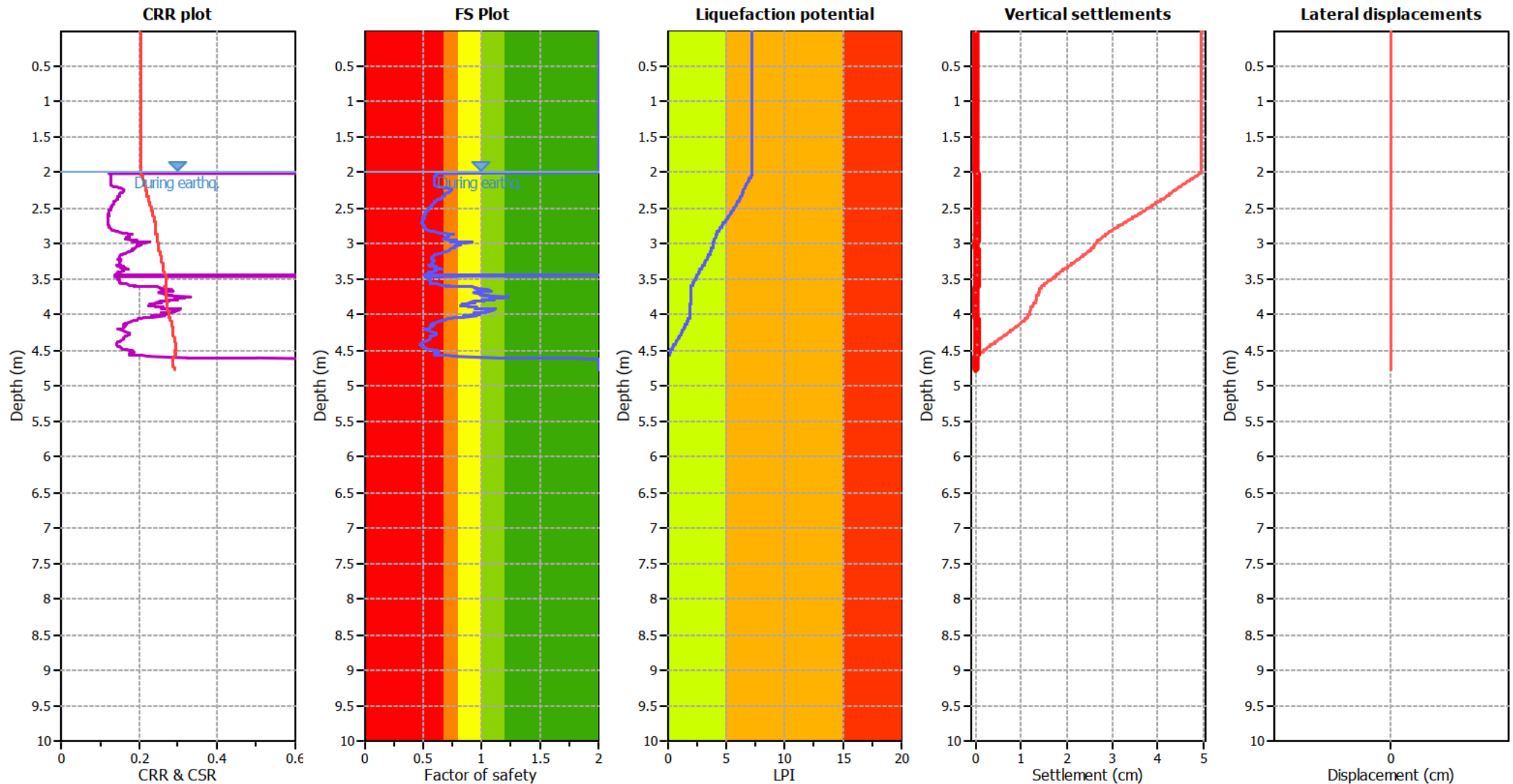
F.S. color scheme

■	Almost certain it will liquefy
■	Very likely to liquefy
■	Liquefaction and no liq. are equally likely
■	Unlike to liquefy
■	Almost certain it will not liquefy

LPI color scheme

■	Very high risk
■	High risk
■	Low risk

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (earthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.50	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.35	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	2.00 m	Fill height:	N/A	Limit depth:	10.00 m

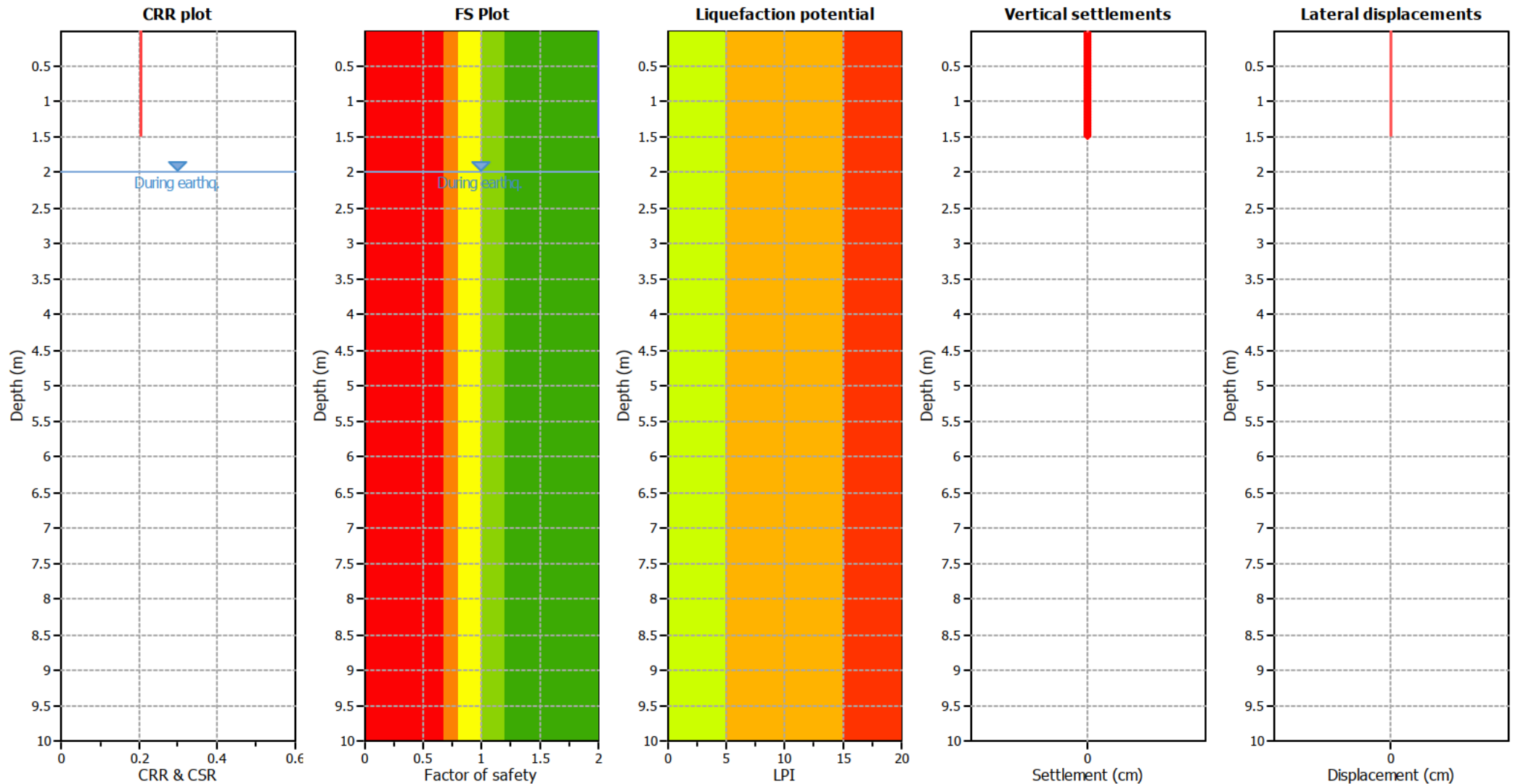
F.S. color scheme

Red	Almost certain it will liquefy
Orange	Very likely to liquefy
Yellow	Liquefaction and no liq. are equally likely
Light Green	Unlike to liquefy
Dark Green	Almost certain it will not liquefy

LPI color scheme

Red	Very high risk
Orange	High risk
Yellow	Low risk

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method: B&I (2014)
 Fines correction method: B&I (2014)
 Points to test: Based on Ic value
 Earthquake magnitude M_w : 7.50
 Peak ground acceleration: 0.35
 Depth to water table (insitu): 2.00 m

Depth to GWT (earthq.): 2.00 m
 Average results interval: 3
 Ic cut-off value: 2.60
 Unit weight calculation: Based on SBT
 Use fill: No
 Fill height: N/A

Fill weight: N/A
 Transition detect. applied: No
 K_{σ} applied: Yes
 Clay like behavior applied: Sands only
 Limit depth applied: Yes
 Limit depth: 10.00 m

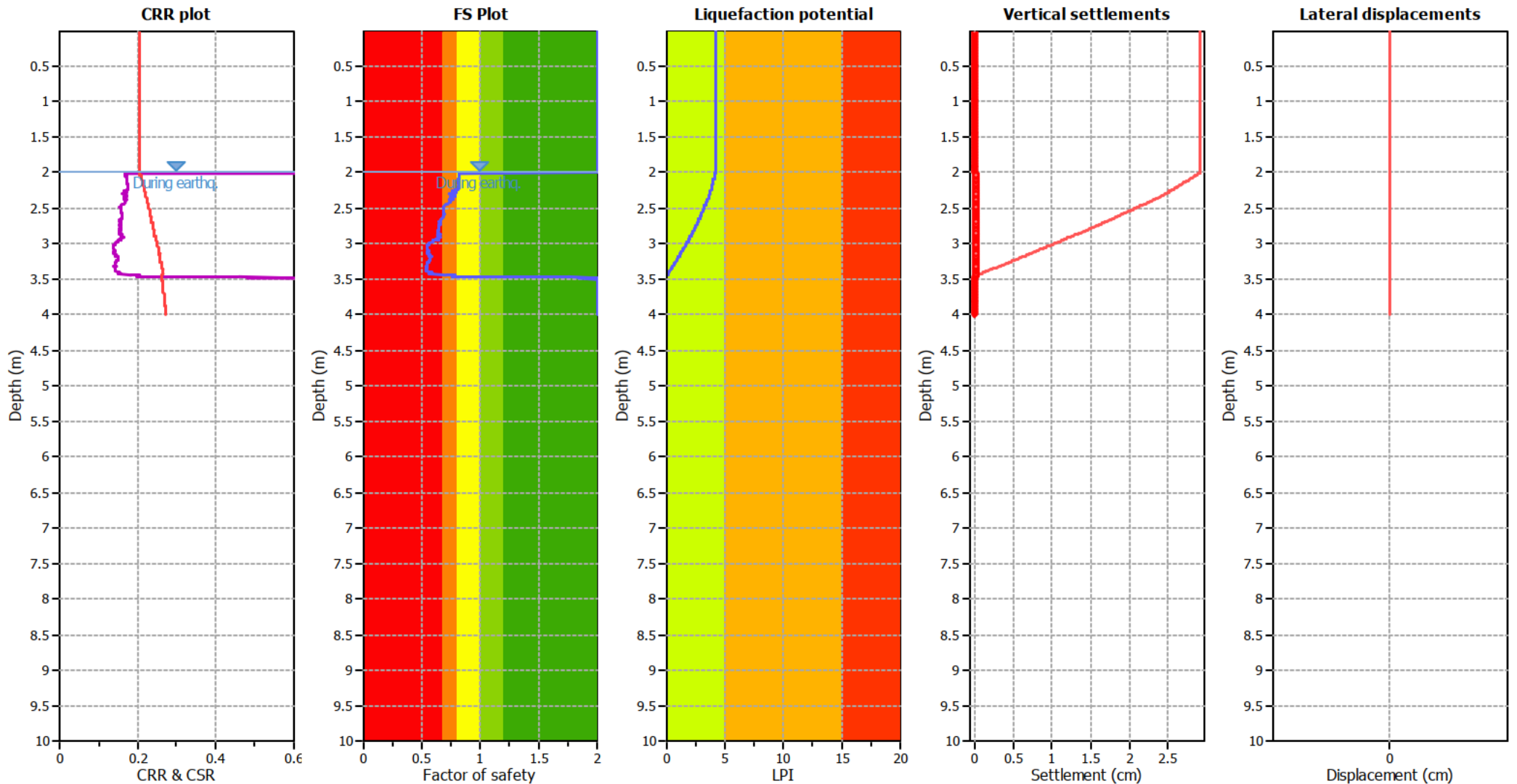
F.S. color scheme

■ Almost certain it will liquefy
■ Very likely to liquefy
■ Liquefaction and no liq. are equally likely
■ Unlike to liquefy
■ Almost certain it will not liquefy

LPI color scheme

■ Very high risk
■ High risk
■ Low risk

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (earthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K ₀ applied:	Yes
Earthquake magnitude M _w :	7.50	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.35	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	2.00 m	Fill height:	N/A	Limit depth:	10.00 m

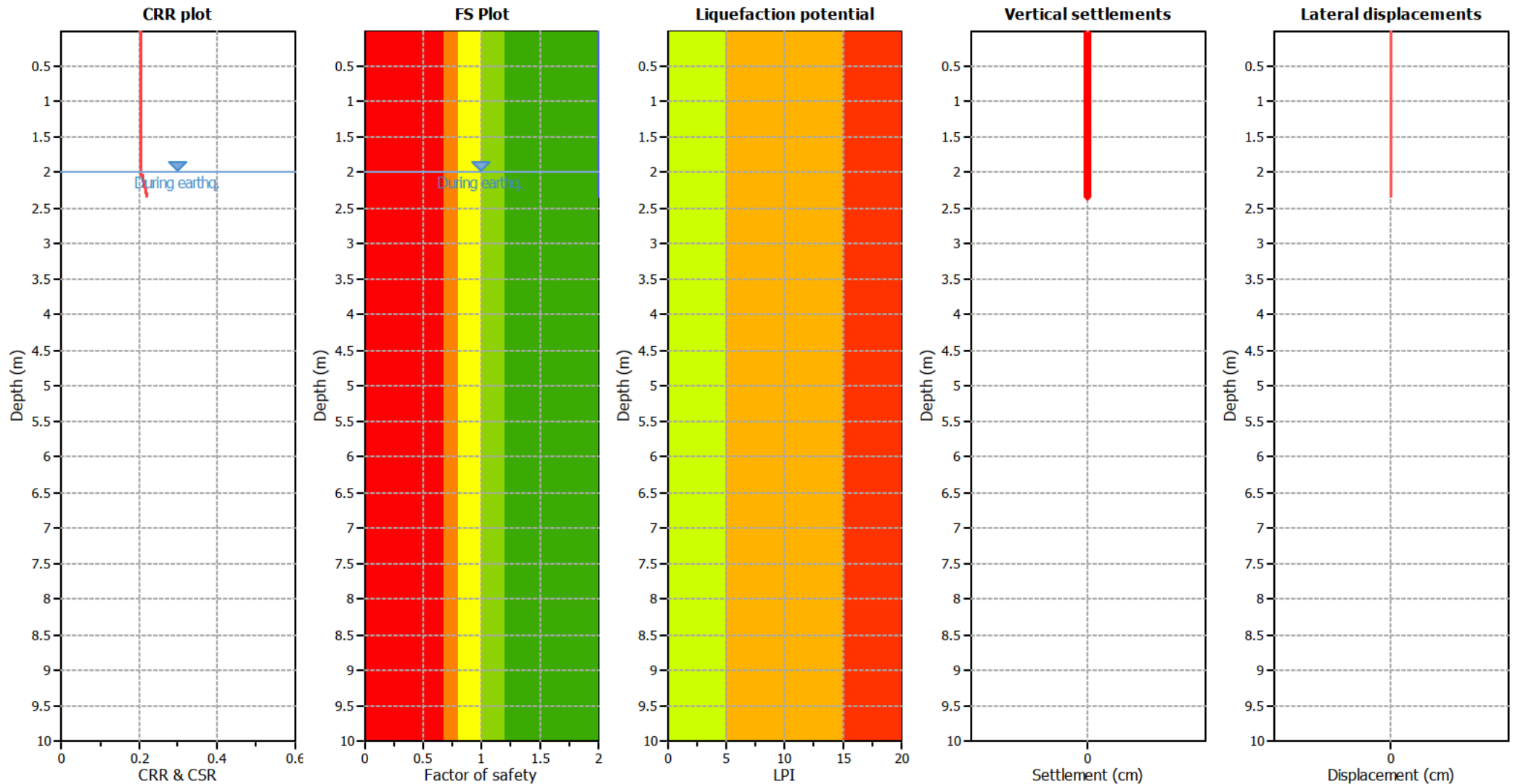
F.S. color scheme

- Almost certain it will liquefy
- Very likely to liquefy
- Liquefaction and no liq. are equally likely
- Unlike to liquefy
- Almost certain it will not liquefy

LPI color scheme

- Very high risk
- High risk
- Low risk

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method: B&I (2014)
 Fines correction method: B&I (2014)
 Points to test: Based on I_c value
 Earthquake magnitude M_w : 7.50
 Peak ground acceleration: 0.35
 Depth to water table (insitu): 2.00 m

Depth to GWT (earthq.): 2.00 m
 Average results interval: 3
 I_c cut-off value: 2.60
 Unit weight calculation: Based on SBT
 Use fill: No
 Fill height: N/A

Fill weight: N/A
 Transition detect. applied: No
 K_{σ} applied: Yes
 Clay like behavior applied: Sands only
 Limit depth applied: Yes
 Limit depth: 10.00 m

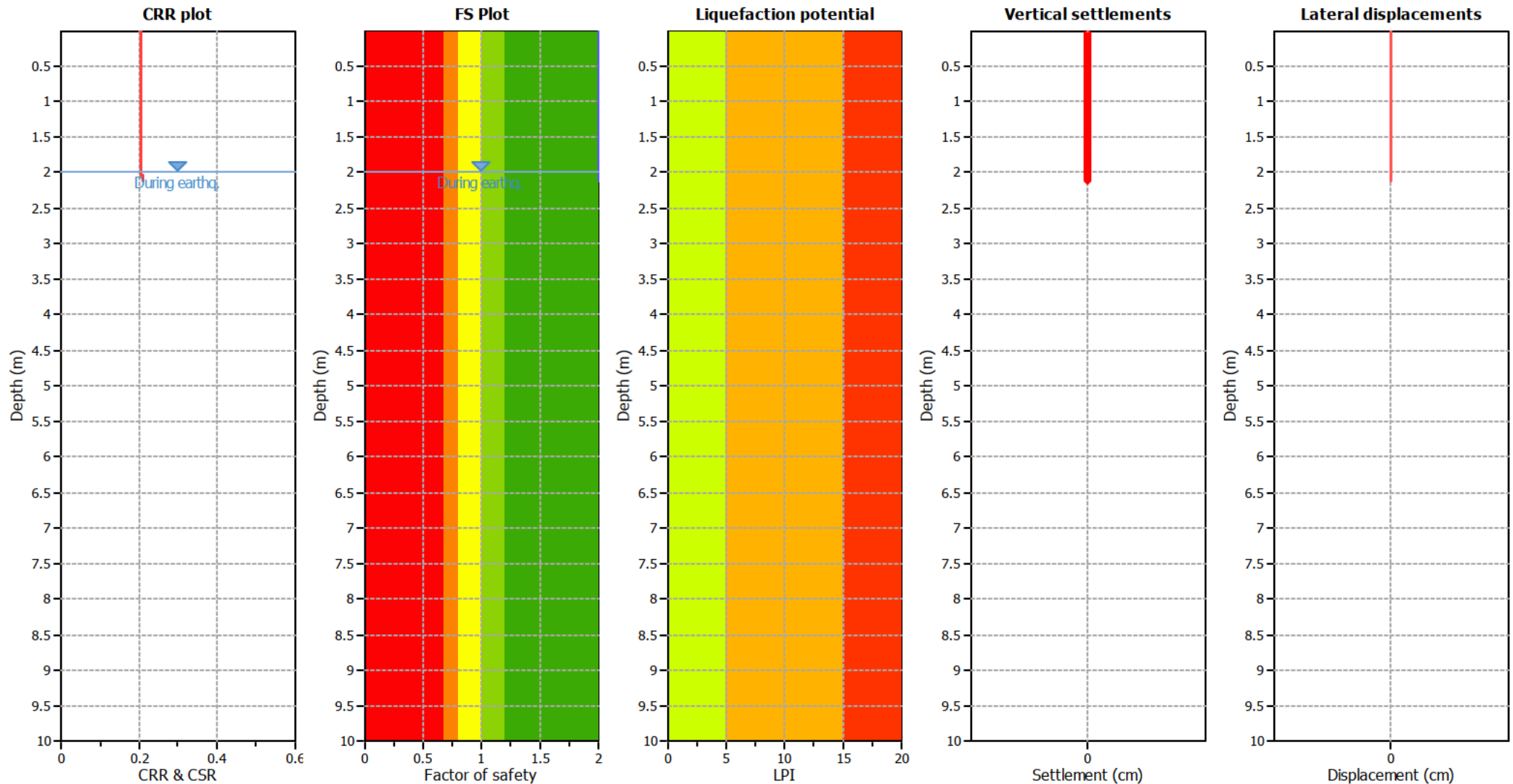
F.S. color scheme

■ Almost certain it will liquefy
■ Very likely to liquefy
■ Liquefaction and no liq. are equally likely
■ Unlike to liquefy
■ Almost certain it will not liquefy

LPI color scheme

■ Very high risk
■ High risk
■ Low risk

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (earthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_{σ} applied:	Yes
Earthquake magnitude M_w :	7.50	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.35	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	2.00 m	Fill height:	N/A	Limit depth:	10.00 m

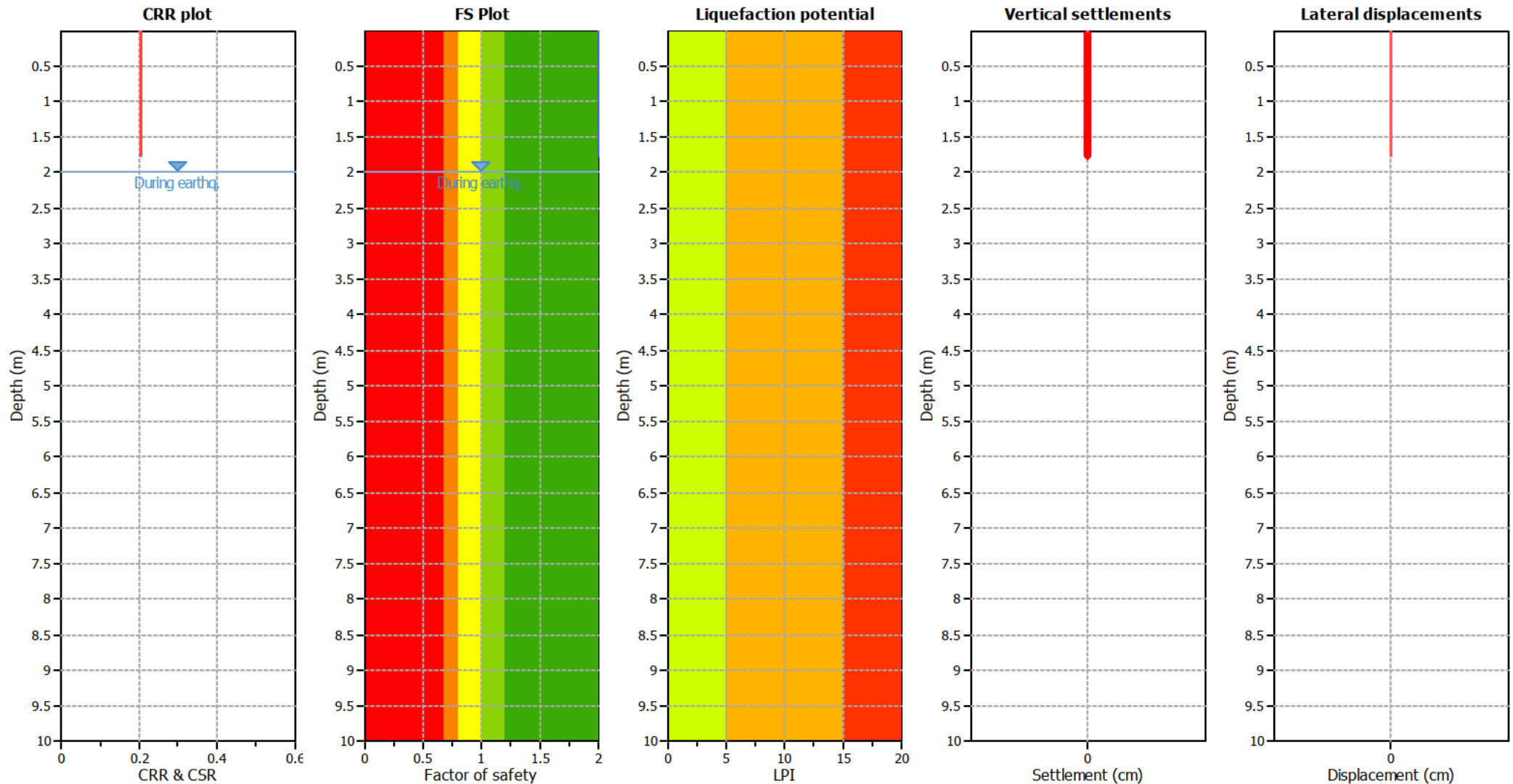
F.S. color scheme

■	Almost certain it will liquefy
■	Very likely to liquefy
■	Liquefaction and no liq. are equally likely
■	Unlike to liquefy
■	Almost certain it will not liquefy

LPI color scheme

■	Very high risk
■	High risk
■	Low risk

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method: B&I (2014)
 Fines correction method: B&I (2014)
 Points to test: Based on Ic value
 Earthquake magnitude M_w : 7.50
 Peak ground acceleration: 0.35
 Depth to water table (insitu): 2.00 m

Depth to GWT (earthq.): 2.00 m
 Average results interval: 3
 Ic cut-off value: 2.60
 Unit weight calculation: Based on SBT
 Use fill: No
 Fill height: N/A

Fill weight: N/A
 Transition detect. applied: No
 K_0 applied: Yes
 Clay like behavior applied: Sands only
 Limit depth applied: Yes
 Limit depth: 10.00 m

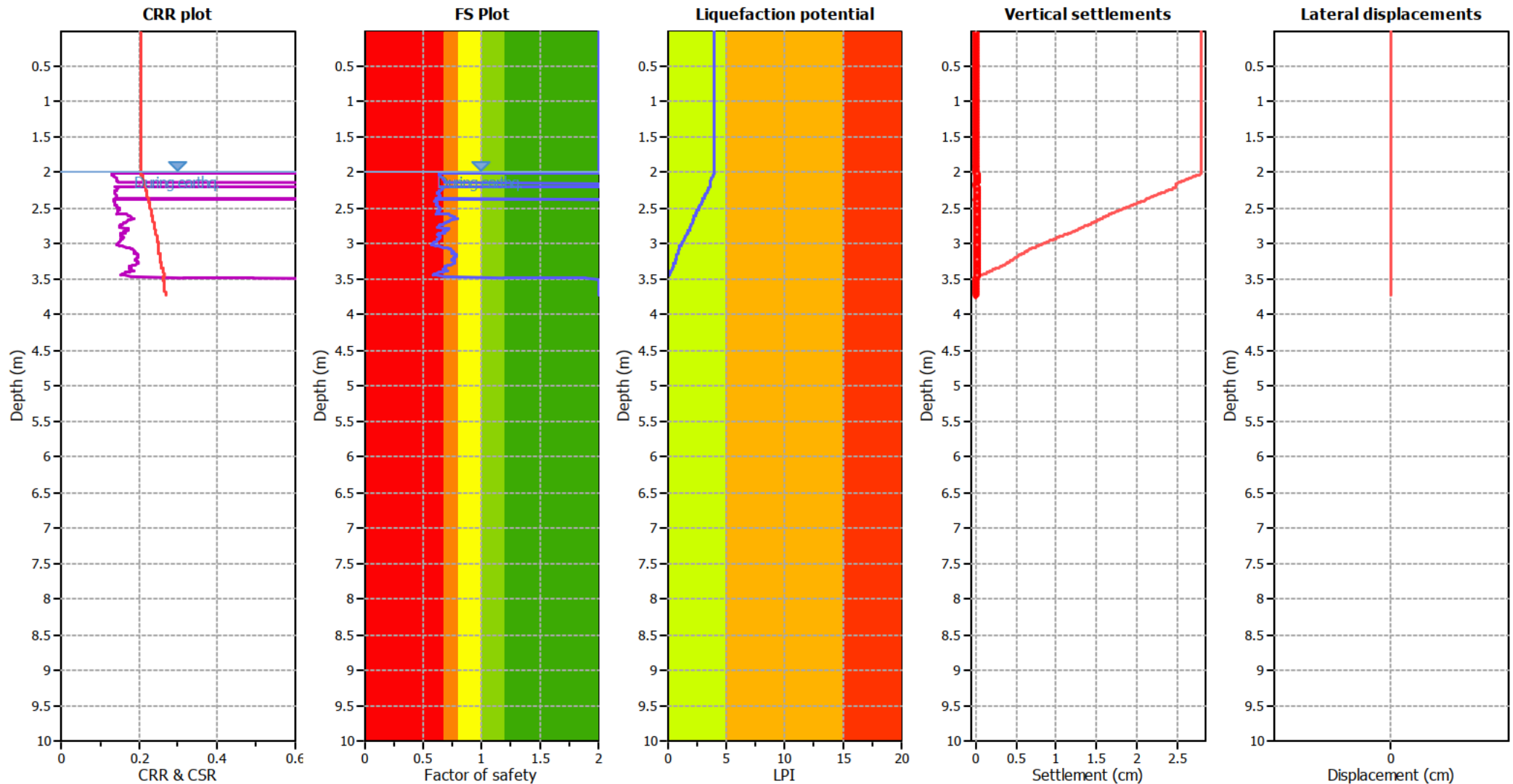
F.S. color scheme

■ Almost certain it will liquefy
■ Very likely to liquefy
■ Liquefaction and no liq. are equally likely
■ Unlike to liquefy
■ Almost certain it will not liquefy

LPI color scheme

■ Very high risk
■ High risk
■ Low risk

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method: B&I (2014)
 Fines correction method: B&I (2014)
 Points to test: Based on Ic value
 Earthquake magnitude M_w : 7.50
 Peak ground acceleration: 0.35
 Depth to water table (insitu): 2.00 m

Depth to GWT (earthq.): 2.00 m
 Average results interval: 3
 Ic cut-off value: 2.60
 Unit weight calculation: Based on SBT
 Use fill: No
 Fill height: N/A

Fill weight: N/A
 Transition detect. applied: No
 K_s applied: Yes
 Clay like behavior applied: Sands only
 Limit depth applied: Yes
 Limit depth: 10.00 m

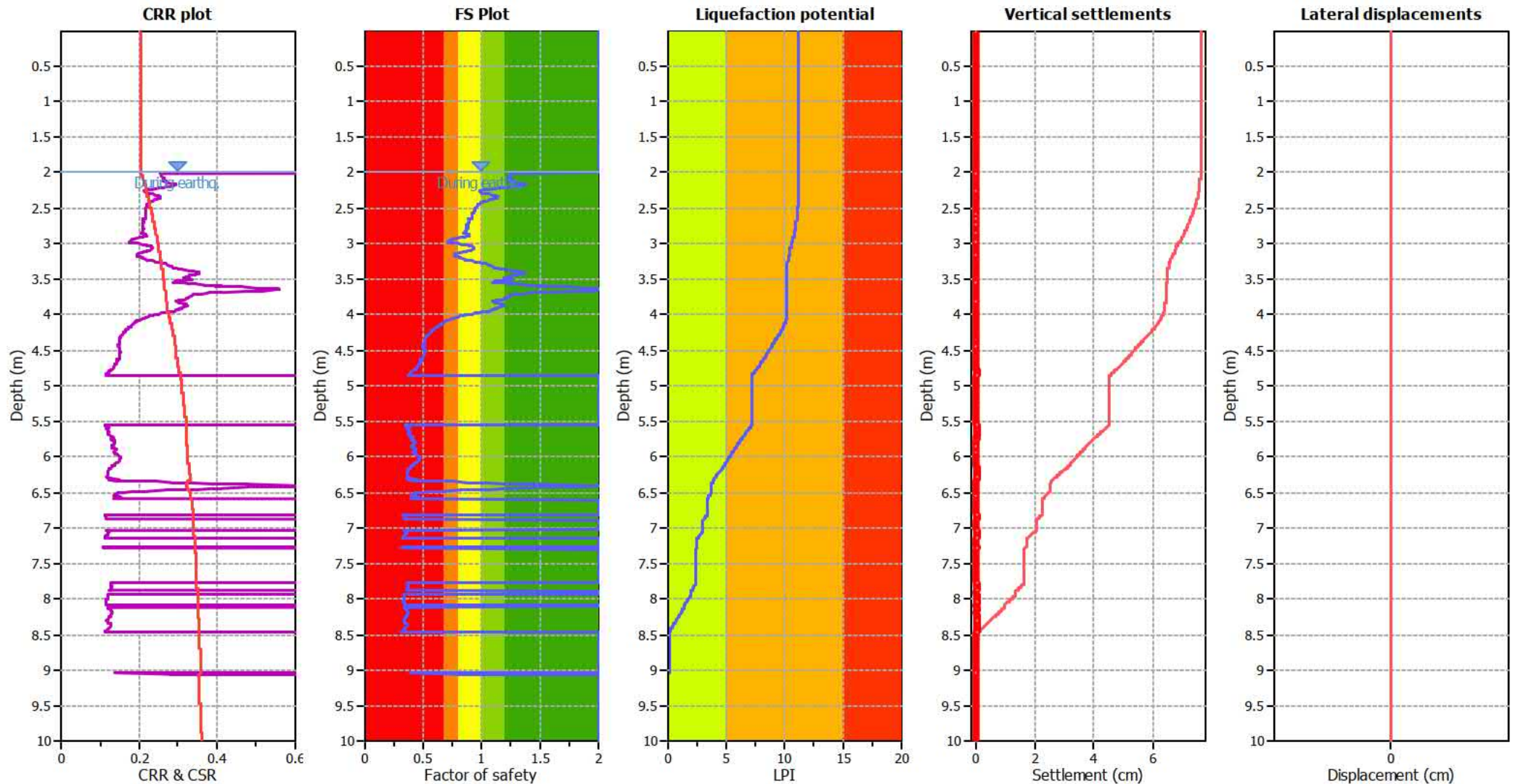
F.S. color scheme

■ Almost certain it will liquefy
■ Very likely to liquefy
■ Liquefaction and no liq. are equally likely
■ Unlike to liquefy
■ Almost certain it will not liquefy

LPI color scheme

■ Very high risk
■ High risk
■ Low risk

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method: B&I (2014)
 Fines correction method: B&I (2014)
 Points to test: Based on Ic value
 Earthquake magnitude M_w : 7.50
 Peak ground acceleration: 0.35
 Depth to water table (insitu): 2.00 m

Depth to GWT (erthq.): 2.00 m
 Average results interval: 3
 Ic cut-off value: 2.60
 Unit weight calculation: Based on SBT
 Use fill: No
 Fill height: N/A

Fill weight: N/A
 Transition detect. applied: No
 K_s applied: Yes
 Clay like behavior applied: Sands only
 Limit depth applied: Yes
 Limit depth: 10.00 m

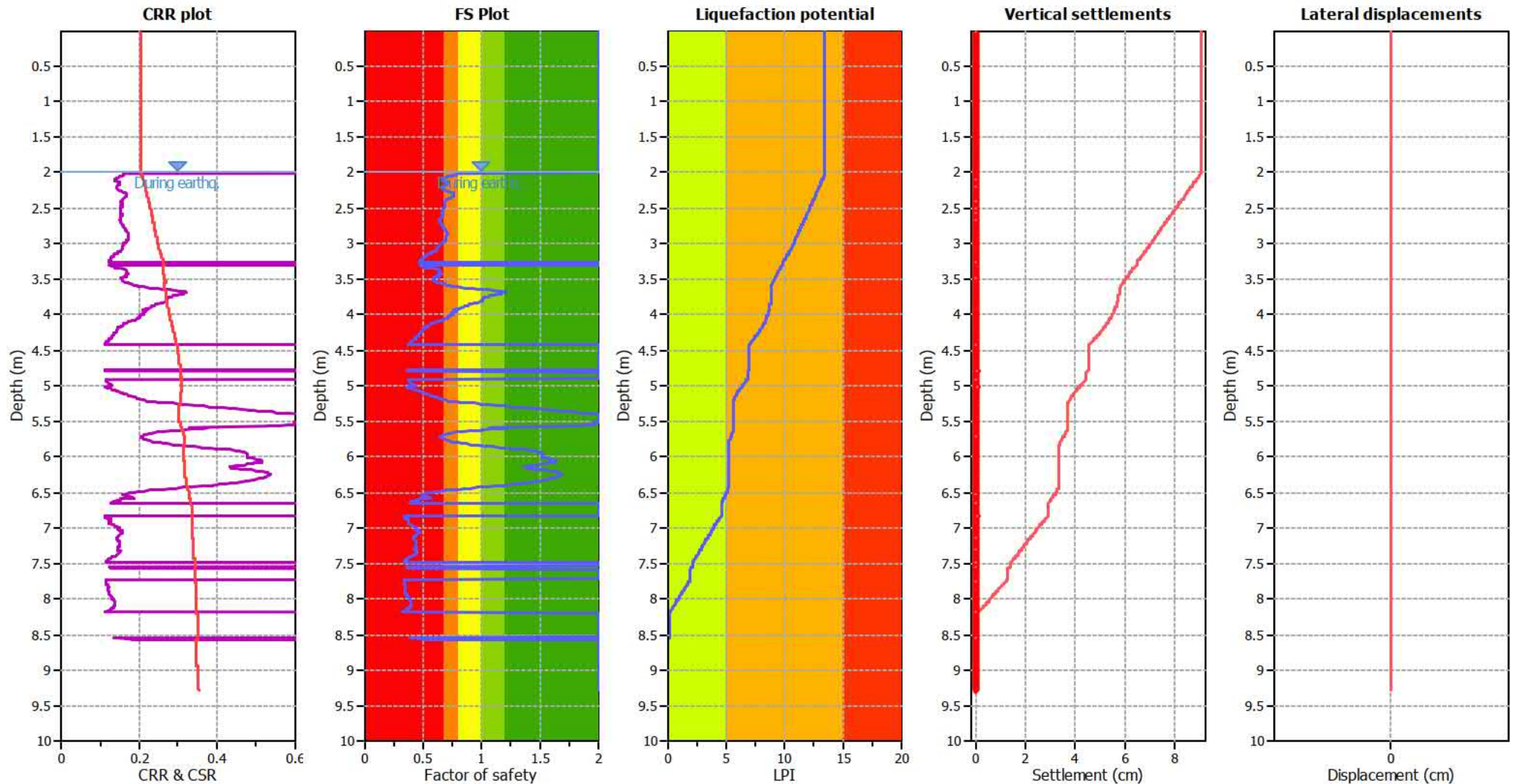
F.S. color scheme

■ Almost certain it will liquefy
■ Very likely to liquefy
■ Liquefaction and no liq. are equally likely
■ Unlike to liquefy
■ Almost certain it will not liquefy

LPI color scheme

■ Very high risk
■ High risk
■ Low risk

Liquefaction analysis overall plots



Input parameters and analysis data

Analysis method:	B&I (2014)	Depth to GWT (erthq.):	2.00 m	Fill weight:	N/A
Fines correction method:	B&I (2014)	Average results interval:	3	Transition detect. applied:	No
Points to test:	Based on Ic value	Ic cut-off value:	2.60	K_s applied:	Yes
Earthquake magnitude M_w :	7.50	Unit weight calculation:	Based on SBT	Clay like behavior applied:	Sands only
Peak ground acceleration:	0.35	Use fill:	No	Limit depth applied:	Yes
Depth to water table (insitu):	2.00 m	Fill height:	N/A	Limit depth:	10.00 m

F.S. color scheme

Red	Almost certain it will liquefy
Orange	Very likely to liquefy
Yellow	Liquefaction and no liq. are equally likely
Green	Unlike to liquefy
Dark Green	Almost certain it will not liquefy

LPI color scheme

Red	Very high risk
Orange	High risk
Yellow	Low risk

Project title : Birches Village - ULS assessment

Location : Prebbleton, Christchurch

Overall vertical settlements report

