

7 to 183 Two Chain Road Plan Change

Geotechnical Assessment Report

Two Chain Road Ltd



Reference: 773-CHCGE291116

24 August 2021

TWO CHAIN ROAD PLAN CHANGE

Geotechnical Assessment Report

Report reference number: 773-CHCGE291116

24 August 2021

PREPARED FOR

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QUALITY INFORMATION

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Revision	Description	Date	Author	Reviewer	Approver
V0	GAR	24/08/21	CT	KWH	CT

Distribution

Report Status	No. of copies	Format	Distributed to	Date
Final	1	PDF	Bruce Van Duyn	24/08/21

EXECUTIVE SUMMARY¹

Two Chain Road Ltd has engaged Tetra Tech Coffey (NZ) Limited to carry out a geotechnical assessment of suitability for the proposed Plan Change and future subdivision of 7 to 183 Two Chain Road, Rolleston, Canterbury. The purpose of this report is to support a Plan Change application for the construction of industrial Lots at the site.

The site investigations and preliminary liquefaction assessment indicates that the site is TC1-like. Other geotechnical hazards (erosion, slippage and inundation) are considered low to very low risk with appropriate future engineering design.

Our assessment has considered the items required by Section 106 of the RMA and in our opinion the site is considered geotechnically suitable for Plan Change and future subdivision. Further investigations and design will need to be carried out at the subdivision consent stage.

¹ This executive summary must be read in the context of the full report and the attached limitations.

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1. INTRODUCTION

Two Chain Road Ltd has engaged Tetra Tech Coffey (NZ) Limited to carry out a geotechnical investigation and assessment of suitability for the proposed Plan Change and future subdivision of 7 to 183 Two Chain Road in Rolleston, Canterbury. The purpose of this report is to support a Plan Change application for the construction of industrial Lots at the site.

Our assessment has considered the items required by Section 106 of the RMA and in our opinion the site is considered geotechnically suitable for Plan Change and future subdivision. Further investigations and design will need to be carried out at the subdivision consent stage.

2. SCOPE

A scope of assessment work for the approximately 98 Ha total area of the site was developed and carried out by Tetra Tech Coffey, as outlined below:

- Review of previous geotechnical investigations including previous work on the site and surrounding area.
- Site walkover to assess geotechnical hazards.
- Assessment of the geotechnical hazards at the site per Section 106 of the RMA.
- Geotechnical analyses and reporting.

Tetra Tech Coffey have considered the following in the preparation of this report:

- Existing geotechnical investigation data available from the New Zealand Geotechnical Database (NZGD) and Environment Canterbury well database.
- Project correspondence with the wider Plan Change consultants engaged by Two Chain Road Ltd.

Reference has also been made to the MBIE Guidance Part D: Subdivisions, to confirm that the requirements outlined in these documents have been incorporated in this report.

3. PROPOSED DEVELOPMENT

The proposed Plan Change area comprises 13 land parcels totalling approximately 98 Ha located to the north of Rolleston. The Plan Change area is bordered by Two Chain Road, Walkers Road, and the Main South and Midland Lines (railways). State Highway 1 (SH1) is located to the southeast of the site, beyond the Main South Line.

The site is predominantly flat and is currently a mixture of grazing and rural residential properties.

We understand that the current proposal is to rezone the land for industrial usage.

4. SITE INVESTIGATION

The location of the geotechnical investigations carried out on / near the site to develop the ground model is provided in Figure 1 (in Appendix A) and are summarised below. Investigation logs are presented in Appendix B.

Table 1: Two Chain Road investigation data

Reference	Depth of test (metres below ground level)	Termination criteria	Reference	Depth of test (metres below ground level)	Termination criteria
S&R TP01	2.4	Target depth	M36/0026	56.1	Target depth
S&R TP06	3.0	Target depth	M36/0030	55.5	Target depth
S&R TP07	2.8	Target depth	M36/0084	35.0	Target depth
TP_153918	2.0	Target depth	M36/3064	55.4	Target depth
TP_153919	2.0	Target depth	M36/5330	46.0	Target depth
TP_153920	2.0	Target depth	M36/4984	54.0	Target depth
HA_34759	0.4	Refusal	M36/4985	48.0	Target depth
HA_82955	0.35	Refusal	M36/4986	48.0	Target depth
HA_153328	0.9	Refusal	M36/5120	43.0	Target depth
HA_48088	0.3	Refusal	M36/5139	39.5	Target depth
HA_48096	0.2	Refusal	M36/5525	47.0	Target depth
HA_48117	0.2	Refusal			

The test pit and hand auger logs have been sourced from the NZGD. ECan well logs have been sourced from <https://www.ecan.govt.nz/data/well-search/>. In addition to the tests noted in Table 1, more than 50 DCP tests and hand augered boreholes have been carried out around the site, however, these have not been included for clarity of the plans as they generally indicate very similar ground conditions.

5. SITE PERFORMANCE

5.1 GROUND MOTION

The site is not in an area mapped for ground damage effects as part of the Canterbury Earthquake Sequence response. A report commissioned by ECan² mapped the site as being in an area where 'damaging liquefaction is unlikely'. An extract from the ECan report is shown in Figure 1 below with the site location indicated.

² ECan (2012), Review of liquefaction hazard information in Eastern Canterbury, including Christchurch City, and parts of Selwyn, Waimakariri and Hurunui Districts, ref. R12/83

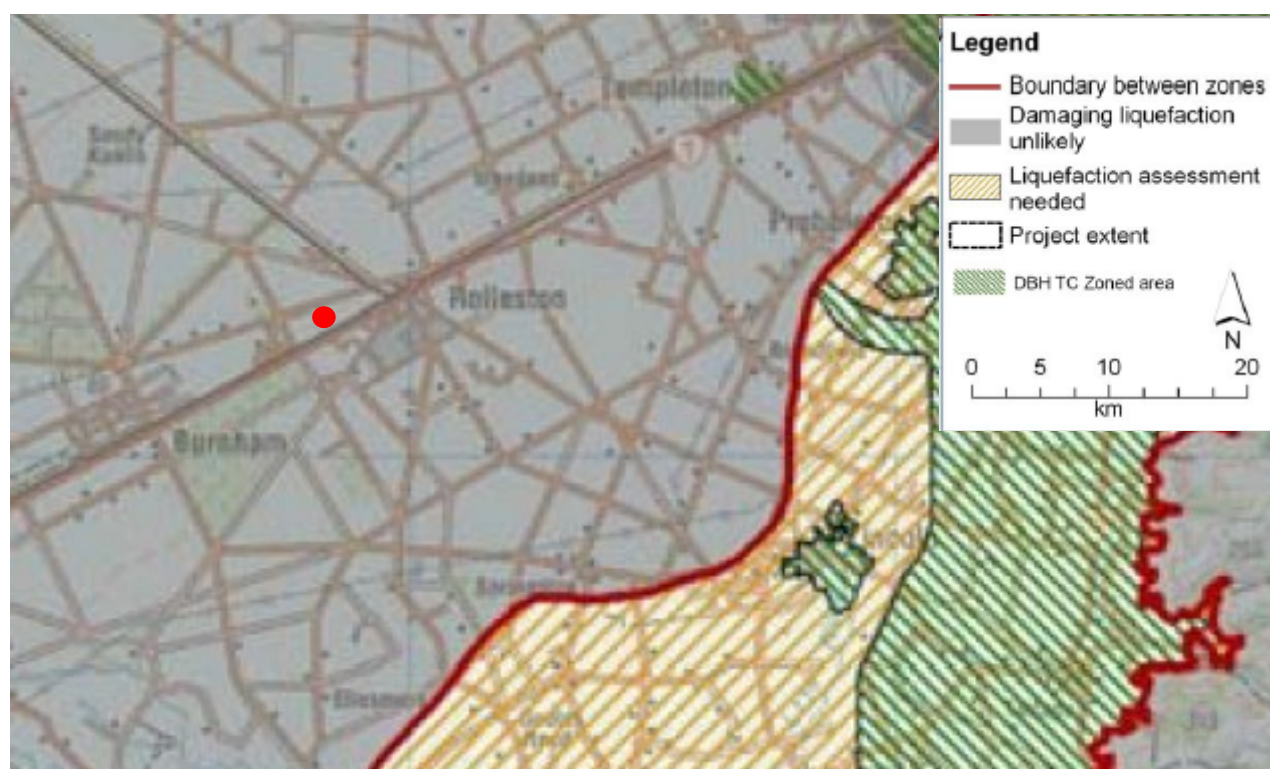


Figure 1: Extract from ECan liquefaction report (site location marked with red dot)

6. GROUND MODEL

6.1 GEOLOGY

The geological map³ of the area indicates that the southwestern half of the site is underlain by “Brownish-grey river alluvium (Q2a)” and northeastern half is underlain by “Grey river alluvium beneath plains and low level terraces (Q1a)”.

6.2 GROUNDWATER

Based on the nearby well logs, groundwater was encountered between 7.5m and 13mbgl. We consider these groundwater levels to be relatively consistent and representative of the general area.

6.3 SUBSURFACE PROFILE

A summary of the ground model for the site is provided below:

Table 2: 7 to 183 Two Chain Road ground profile

Description	Strength/consistency	Thickness (m)	Depth to top of layer (mbgl)
Silt (topsoil)	N/A	0.15 to 0.2	0.0
Silt with some sand and gravel	Stiff to hard	0.3 to 0.65	0.15 to 0.35
Sandy Gravel, with minor silt lenses	Dense to very dense	>30	0.3 to 0.9

³ Forsyth, P.J.; Barrell, D.J.A.; Jongens, R. (compilers) 2008: Geology of the Christchurch area: scale 1:250,000. Lower Hutt: GNS Science. Institute of Geological & Nuclear Sciences 1:250,000 geological map 16. 67 p. + 1 folded map

6.4 SITE SUB-SOIL CLASS

In accordance with NZS1170.5, Section 3.1.3, a subsoil classification of “Class D – Deep or soft soil sites” can be assumed for the site.

7. GEOTECHNICAL HAZARD ASSESSMENT

7.1 EROSION

The site has relatively flat topography and is bounded by existing roads and the rail lines. Provided appropriate stormwater systems are installed as part of the development, there will be few viable sources of erosion at this site.

7.2 FALLING DEBRIS

As there are no slopes or exposed hills or rock faces surrounding the site, there are no sources of falling debris at the site, or for the surrounding area.

7.3 SUBSIDENCE

7.3.1 Liquefaction induced settlement

Saturated, loose, uniform fine grained alluvial soils are subject to seismic (liquefaction-induced) settlement during a significant earthquake. Liquefaction typically affects saturated, loose granular soils ranging from sandy silts to sands, but seismic shaking can also result in strength losses in fine-grained, cohesive soils. Liquefaction does not occur in dense, well-graded alluvial gravel soils that are present at this site.

Due to the dense nature of the gravel encountered, liquefaction risk is considered to be negligible for this project. Although not relevant for industrial development, for comparison purposes, the site could be considered TC1-like.

7.3.2 Static settlement

Settlement is a crucial factor that can cause structure serviceability issues. Static load-induced settlement typically occurs in low-lying areas underlain by soft, compressible soils as a result of increased overburden loads. As the site is underlain by dense river gravels, static settlement is not deemed a hazard for the site provided any earthworks are carried out to the relevant standards.

7.4 SLIPPAGE

We have not observed any sources of land instability on the site and due to the flat site topography, we consider the risk of slope failure to be very low. The appropriate design of batter slopes near waterways will mitigate this risk further.

7.5 INUNDATION

In relation to stormwater inundation, we recommend that drainage design and management at the site be addressed by specialist consultants as it is beyond the scope of this report. We expect that with appropriate stormwater and flood control systems, the risk of inundation will be low.

8. CONCLUSIONS

We consider that the site is suitable for development subject to further investigation and design at the subdivision consent stage. Based on the mapped geology and on-site testing carried out to date, the site is considered TC1-like.

Additional geotechnical investigation will be required to refine the ground model and address any geotechnical risks for the proposed Lots once a subdivision plan has been further developed.

9. LIMITATIONS

This report has been prepared solely for the use of our client, Two Chain Road Ltd, their professional advisers and Selwyn District Council (SDC) in relation to the specific project described herein. No liability is accepted in respect of its use for any other purpose or by any other person or entity.

It is recommended that all other parties seek professional geotechnical advice to satisfy themselves as to its on-going suitability for their intended use.

As subsurface information has been obtained from discrete investigation locations, which by their nature only provide information about a relatively small volume of subsoils, there may be special conditions pertaining to this site which have not been disclosed by the investigation and which have not been taken into account in the report. If variations in the subsoils occur from those described or assumed to exist, then the matter should be referred to us immediately.

Please also refer to the enclosed *Important Information about Your Tetra Tech Coffey Report*.

10. CLOSURE

If you have queries or require further clarification regarding aspects of this report, please contact the undersigned.

For and on behalf of Tetra Tech Coffey

Prepared by



Chris Thompson
BSc (Tech)
Associate Engineering Geologist

Reviewed by



Kah-Weng Ho
BE (Hons) CMEngNZ
Senior Principal

IMPORTANT INFORMATION ABOUT YOUR TETRA TECH COFFEY REPORT

As a client of Tetra Tech Coffey you should know that site subsurface conditions cause more construction problems than any other factor. These notes have been prepared by Tetra Tech Coffey to help you interpret and understand the limitations of your report.

Your report is based on project specific criteria

Your report has been developed on the basis of your unique project specific requirements as understood by Tetra Tech Coffey and applies only to the site investigated. Project criteria typically include the general nature of the project; its size and configuration; the location of any structures on the site; other site improvements; the presence of underground utilities; and the additional risk imposed by scope-of-service limitations imposed by the client. Your report should not be used if there are any changes to the project without first asking Tetra Tech Coffey to assess how factors that changed subsequent to the date of the report affect the report's recommendations. Tetra Tech Coffey cannot accept responsibility for problems that may occur due to changed factors if they are not consulted.

Subsurface conditions can change

Subsurface conditions are created by natural processes and the activity of man. For example, water levels can vary with time, fill may be placed on a site and pollutants may migrate with time. Because a report is based on conditions which existed at the time of subsurface exploration, decisions should not be based on a report whose adequacy may have been affected by time. Consult Tetra Tech Coffey to be advised how time may have impacted on the project.

Interpretation of factual data

Site assessment identifies actual subsurface conditions only at those points where samples are taken and when they are taken. Data derived from literature and external data source review, sampling and subsequent laboratory testing are interpreted by geologists, engineers or scientists to provide an opinion about overall site conditions, their likely impact on the proposed development and recommended actions. Actual conditions may differ from those inferred to exist, because no professional, no matter how qualified, can reveal what is hidden by earth, rock and time. The actual interface between materials may be far more gradual or abrupt than assumed based on the facts obtained. Nothing can be done to change the actual site conditions which exist, but steps can be taken to reduce the impact of unexpected conditions. For this reason, owners should retain the services of Tetra Tech Coffey through the development stage, to identify variances, conduct additional tests if required, and recommend solutions to problems encountered on site.

Your report will only give preliminary recommendations

Your report is based on the assumption that the site conditions as revealed through selective point sampling are indicative of actual conditions throughout an area. This assumption cannot be substantiated until project implementation has commenced and therefore your report recommendations can only be regarded as preliminary. Only Tetra Tech Coffey, who prepared the report, is fully familiar with the background information needed to assess whether or not the report's recommendations are valid and whether or not changes should be considered as the project develops. If another party undertakes the implementation of the recommendations of this report there is a risk that the report will be misinterpreted and Tetra Tech Coffey cannot be held responsible for such misinterpretation.

Your report is prepared for specific purposes and persons

To avoid misuse of the information contained in your report it is recommended that you confer with Tetra Tech Coffey before passing your report on to another party who may not be familiar with the background and the purpose of the report. Your report should not be applied to any project other than that originally specified at the time the report was issued.

Interpretation by other design professionals

Costly problems can occur when other design professionals develop their plans based on misinterpretations of a report. To help avoid misinterpretations, retain Tetra Tech Coffey to work with other project design professionals who are affected by the report. Have Tetra Tech Coffey explain the report implications to design professionals affected by them and then review plans and specifications produced to see how they incorporate the report findings.

Data should not be separated from the report

The report as a whole presents the findings of the site assessment and the report should not be copied in part or altered in any way. Logs, figures, drawings, etc. are customarily included in our reports and are developed by scientists, engineers or geologists based on their interpretation of field logs (assembled by field personnel) and laboratory evaluation of field samples. These logs etc. should not under any circumstances be redrawn for inclusion in other documents or separated from the report in any way.

Geoenvironmental concerns are not at issue

Your report is not likely to relate any findings, conclusions, or recommendations about the potential for hazardous materials existing at the site unless specifically required to do so by the client. Specialist equipment, techniques, and personnel are used to perform a geoenvironmental assessment. Contamination can create major health, safety and environmental risks. If you have no information about the potential for your site to be contaminated or create an environmental hazard, you are advised to contact Tetra Tech Coffey for information relating to geoenvironmental issues.

Rely on Tetra Tech Coffey for additional assistance

Tetra Tech Coffey is familiar with a variety of techniques and approaches that can be used to help reduce risks for all parties to a project, from design to construction. It is common that not all approaches will be necessarily dealt with in your site assessment report due to concepts proposed at that time. As the project progresses through design towards construction, speak with Tetra Tech Coffey to develop alternative approaches to problems that may be of genuine benefit both in time and cost.

Responsibility

Reporting relies on interpretation of factual information based on judgement and opinion and has a level of uncertainty attached to it, which is far less exact than the design disciplines. This has often resulted in claims being lodged against consultants, which are unfounded. To help prevent this problem, a number of clauses have been developed for use in contracts, reports and other documents. Responsibility clauses do not transfer appropriate liabilities from Tetra Tech Coffey to other parties but are included to identify where Tetra Tech Coffey's responsibilities begin and end. Their use is intended to help all parties involved to recognise their individual responsibilities. Read all documents from Tetra Tech Coffey closely and do not hesitate to ask any questions you may have.

APPENDIX A: SITE PLAN



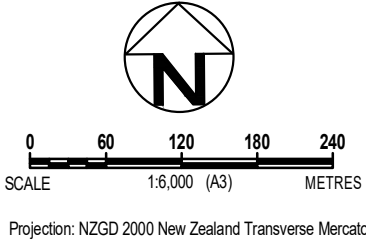
LEGEND

- Test pits
- Hand augers
- Well bore logs
- Contour
- Site boundary

Source & Notes:

Aerial imagery flown 2017 supplied by LINZ
Data licenced for re-use under the Creative Commons Attribution 4.0 New Zealand licence.

revision	no.	description			drawn	approved	date
	A	ORIGINAL ISSUE			RZ	CT	22.07.21




drawn	RZ
approved	CT
date	22.07.2021
scale	AS SHOWN
original size	A3




client: TWO CHAIN ROAD LIMITED		
project: 7 TO 183 TWO CHAIN ROAD		
title: TWO CHAIN ROAD TEST LOCATIONS		
project no: 773-CHCGE291116	figure no: 01	rev: A

APPENDIX B: INVESTIGATION DATA

 www.aurecongroup.com	HAND AUGER RECORD	HOLE NO.	HA2	
		PROJECT NO.	224926	
PROJECT Stonebrook Stage 10 - Lot 196				
CLIENT CDL LAND NZ LTD	CO-ORDINATES (NZTM) E 1548079 N 5172400	SHEET	1	of 1
METHOD HA		DATE from 08/10/2014	to	08/10/2014
MACHINE & NO. NA	ORIENTATION VERTICAL	GROUND-LEVEL	+60.00	m RL


Water level	Tests	Samples			Reduced Level	Depth (m)	Legend	STRATA DESCRIPTION
		Type	Ref	Depth				SUBORDINATE FRACTION, MAJOR FRACTION, MINOR FRACTION, COLOUR, STRUCTURE, STRENGTH, MOISTURE CONDITION GRADING, BEDDING, PLASTICITY, ETC.... (NZ GEOTECHNICAL SOCIETY - FIELD DESCRIPTION OF SOIL AND ROCK)
		↑ HA ↓		0.00				SILT , some fine to coarse sand, minor fine to coarse gravel, dark brown. "Stiff", moist, low plasticity (TOPSOIL).
					+59.70	0.30		End of Hand Auger at 0.30m, on 08/10/2014 <i>Termination Reason:</i> Due to Inferred Gravel.


<ul style="list-style-type: none"> Small Disturbed Sample Large Disturbed Sample SPT Liner Sample Thin Wall Undisturbed Sample U100 Undisturbed Sample Pocket Penetrometer Test Piston Sample 	<ul style="list-style-type: none"> Water Level Impression Packer Test Standard Penetration Test Permeability Test Piezometer / Standpipe Tip Packer Test In-situ Vane Shear Test 	<p>LOGGED <u>M. TIWEKA</u></p> <p>DATE <u>08/10/2014</u></p> <p>CHECKED <u>R. SMITH</u></p> <p>DATE <u>09/10/2014</u></p>	<p>REMARKS</p> <p>Coordinates approximated from CERA public viewer using post-earthquake aerial imagery (24/12/2011) accurate to +/- 1.0m.</p> <p>Ground level approximated from vertical LiDAR data accurate to +/- 1.0m; based on Lyttelton Vertical Datum.</p> <p>Groundwater was not encountered.</p>
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 www.aurecongroup.com	HAND AUGER RECORD	HOLE NO.	HA2	
		PROJECT NO.	224926	
PROJECT Stonebrook Stage 10 - Lot 199				
CLIENT CDL LAND NZ LTD	CO-ORDINATES (NZTM) E 1548023 N 5172371	SHEET	1	of 1
METHOD HA		DATE from 08/10/2014	to	08/10/2014
MACHINE & NO. NA	ORIENTATION VERTICAL	GROUND-LEVEL	+60.00	m RL

[illegible]

<ul style="list-style-type: none"> Small Disturbed Sample Large Disturbed Sample SPT Liner Sample Thin Wall Undisturbed Sample U100 Undisturbed Sample Pocket Penetrometer Test Piston Sample 	<ul style="list-style-type: none"> Water Level Impression Packer Test Standard Penetration Test Permeability Test Piezometer / Standpipe Tip Packer Test In-situ Vane Shear Test 	<p>LOGGED <u>M. TIWEKA</u></p> <p>DATE <u>08/10/2014</u></p> <p>CHECKED <u>R. SMITH</u></p> <p>DATE <u>09/10/2014</u></p>	<p>REMARKS</p> <p>Coordinates approximated from CERA public viewer using post-earthquake aerial imagery (24/12/2011) accurate to +/- 1.0m.</p> <p>Ground level approximated from vertical LiDAR data accurate to +/- 1.0m; based on Lyttelton Vertical Datum.</p> <p>Groundwater was not encountered.</p>
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<div> www.aurecongroup.com</div>	HAND AUGER RECORD	HOLE NO.	HA2	
		PROJECT NO.	224926	
PROJECT Stonebrook Stage 10 - Lot 201				
CLIENT CDL LAND NZ LTD	CO-ORDINATES (NZTM) E 1547985 N 5172350	SHEET	1	of 1
METHOD HA		DATE from 08/10/2014	to	08/10/2014
MACHINE & NO. NA	ORIENTATION VERTICAL	GROUND-LEVEL	+60.00	m RL

Water level	Tests	Samples			Reduced Level	Depth (m)	Legend	STRATA DESCRIPTION SUBORDINATE FRACTION, MAJOR FRACTION, MINOR FRACTION, COLOUR, STRUCTURE, STRENGTH, MOISTURE CONDITION GRADING, BEDDING, PLASTICITY, ETC... (NZ GEOTECHNICAL SOCIETY - FIELD DESCRIPTION OF SOIL AND ROCK)
		Type	Ref	Depth				
		HA		0.00	+59.80	0.20		SILT , some fine to coarse sand, minor fine to coarse gravel, dark brown. "Very stiff", moist, low plasticity (TOPSOIL).
								End of Hand Auger at 0.20m, on 08/10/2014 <i>Termination Reason:</i> Due to Inferred Gravel.

<ul style="list-style-type: none"> Small Disturbed Sample Large Disturbed Sample SPT Liner Sample Thin Wall Undisturbed Sample U100 Undisturbed Sample Pocket Penetrometer Test Piston Sample 	<ul style="list-style-type: none"> Water Level Impression Packer Test Standard Penetration Test Permeability Test Piezometer / Standpipe Tip Packer Test In-situ Vane Shear Test 	<p>LOGGED <u>M. TIWEKA</u></p> <p>DATE <u>08/10/2014</u></p> <p>CHECKED <u>R. SMITH</u></p> <p>DATE <u>09/10/2014</u></p>	<p>REMARKS</p> <p>Coordinates approximated from CERA public viewer using post-earthquake aerial imagery (24/12/2011) accurate to +/- 1.0m.</p> <p>Ground level approximated from vertical LiDAR data accurate to +/- 1.0m; based on Lyttelton Vertical Datum.</p> <p>Groundwater was not encountered.</p>
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REPORT OF INVESTIGATION: GA_6663

SHEET: 1 OF 1

LOCATION: Lot 155 Fairfield Way

COORDS: 1548454 mE 5172599 mN
SURFACE RL: 56.68 m DATUM: MSL
TEST DEPTH: 0.60 m

CONTRACTOR: GOLDER
MACHINE: Hand Auger / Dynamic Cone Penetrometer
RECORDED: LW DATE: -
CHECKED: RS DATE: -

Formation	Graphic Log	Description	USC	Moisture Condition	Consistency / Density	Water Observations	Depth (m)	Blows per 100 mm	Backfill
		TOPSOIL with minor subrounded medium gravels, dark brown, soft, dry, some rootlets Clayey SILT, mixed with topsoil with minor subrounded gravels, dark-light brown, soft to firm, dry, low plasticity	OL ML	D	S S-F	Groundwater not encountered			
End of hole at: 0.4 m							0.5	End of test at: 0.60 m	

Remarks:

DCP Termination: Refusal.

Notes:
Coordinates and elevation are estimates only.
This report of penetrometer must be read in conjunction with accompanying notes and abbreviations. It has been prepared for geotechnical purposes only, without attempt to assess possible contamination. Any references to potential contamination are for information only and not necessarily indicate the presence or absence of soil or groundwater contamination.
Hand auger: Logged in accordance with NZGS guideline "Field description of soil and rock" 2005.
DCP: Performed to NZS:4402, Test 6.5.2:1988.

HAND AUGER AND SCALA LOG				Job No.: 16158	
Client: Trident Group Ltd				Hole No.: HA04/SP04	
Project: Residential Building				Date: 11/05/2016	
Location: 24 Chaucer Street, Rolleston, Christchurch				Logged By: HH	
Coordinates: E 1549472.3, N 5173171.6				Sheet: 1 of 1	


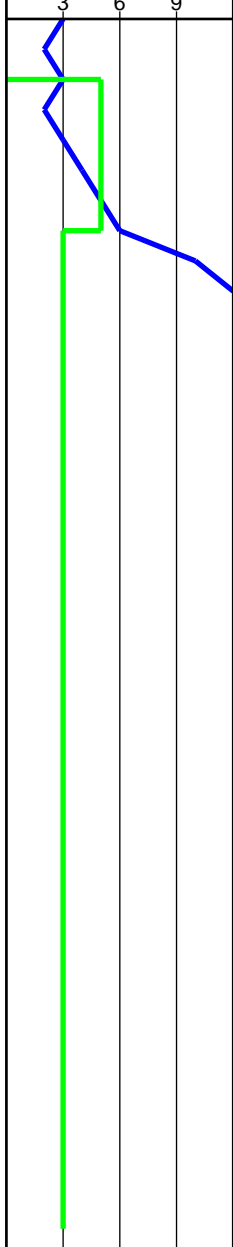
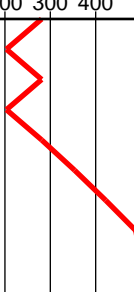
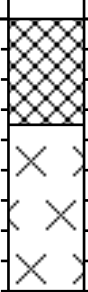
Subsurface Conditions	Depth (m)	Groundwater	Geological Unit	Graphic Log	Scala Penetrometer (blows / 50mm)	Vane Shear Strength (refer notes for details)
SILT with minor gravel and trace sand; light brown; dry; low plasticity. Gravel is fine to medium, subrounded. Sand is fine.		Groundwater Not Encountered	TOPSOIL			
0.4m: End of hole (unable to penetrate)	0.5					


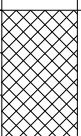
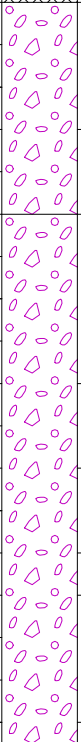
Notes & Abbreviations

Soils logged in accordance with 'The guidelines for the classification and description of soil and rock for engineering purposes' December 2005, NZGS. Co-ordinates are in NZTM unless otherwise specified.


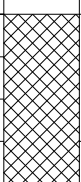
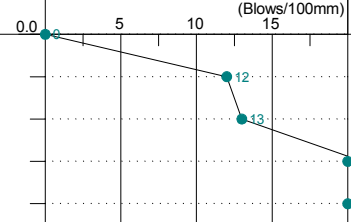
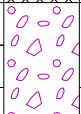
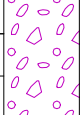
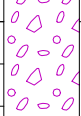
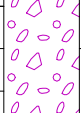
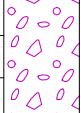

Water	Shear Vane	Other Comments
▼ Standing Water Level ▽ Water Level At Time Of Drilling ↰ Out Flow ↱ In Flow	Corrected as per NZGS Guidelines Vane No.: UTP = Unable To Penetrate + = Peak Exceeded - = No Result	




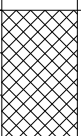

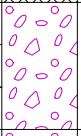
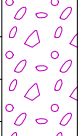
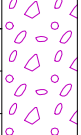

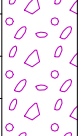

		Project Title: 25 John Street, Rolleston			HA/DCP02					
		Project Number: 20687		Client: Theresa Phelam						
		GL (mAOD):		N Coord: 0		E Coord: 0				
Date: 13/10/2020		Method: Hand Auger/DCP		Logged By: AM		Scale: 1:25 Sheet 1 Of 1				
Blows (per 100mm) 3 6 9		UBC (kPa) (Stockwell) 100 200 300 400		Level	Legend	Depth (m)		Description		Water
						0.35 <				

 Soil & Rock Consultants GEOTECHNICAL & ENVIRONMENTAL ENGINEERS		CLIENT: Lincoln Amor PROJECT: 847 Jones Rd, Rolleston		Test Pit No: TP01 Sheet 1 of 1	
Drill Type: 8t Excavator Drilled By: Soil & Rock Consultants Date Started: 16/12/14 Date Finished: 16/12/14		Project No: C14652 Coordinates: 1549602 E, 5173496 N Ground Elevation: 55m LINZ Topo Water Level: Groundwater not encountered		Logged By: MG Reviewed By: MLB Surface Conditions: Near level, grass Shear Vane Number: N/A	
STRATIGRAPHY	DEPTH (m)	GRAPHIC LOG	Soil description in accordance with the NZ Geotechnical Society Inc 2005 "Guidelines for Field Description of Soil and Rock in Engineering Use"	WATER LEVEL (m)	DEPTH (m)
Fill	0.0		SILT, some fine to medium sub-rounded to rounded gravel, trace to minor fine to medium sand, greyish brown, medium dense to dense, dry to moist, non-plastic		0.0
	0.5		Silty fine to coarse sub-rounded to rounded GRAVEL, minor fine to medium sand, greyish brown, dense to very dense, moist minor to some fine to medium sand		0.5
Alluvial Deposits	1.0		Sandy fine to coarse sub-rounded to rounded GRAVEL, trace to minor silt, trace sub-rounded to rounded cobble, brownish grey, very dense, moist trace silt		1.0
	1.5		greyish brown moist to wet minor sub-rounded to rounded cobble		1.5
	2.0		wet		2.0
	2.5		END OF TEST PIT. 2.4 METRES. [Target Depth]		2.5
	3.0				3.0
COMMENTS:					

TEST PIT LOG C14652_TP1-10.GPJ S+R 2012-AGS - REVISED.GDT 18/12/14

<div><div> Soil & Rock Consultants GEOTECHNICAL & ENVIRONMENTAL ENGINEERS</div></div>			CLIENT: Lincoln Amor			Test Pit No: TP06				
			PROJECT: 847 Jones Rd, Rolleston			Sheet 1 of 1				
Drill Type: 8t Excavator			Project No: C14652			Logged By: MG				
Drilled By: Soil & Rock Consultants			Coordinates: 1549591 E, 5173520 N			Reviewed By: MLB				
Date Started: 16/12/14			Ground Elevation: 55m LINZ Topo			Surface Conditions: Near level, grass				
Date Finished: 16/12/14			Water Level: Groundwater not encountered			Shear Vane Number: N/A				
STRATIGRAPHY		DEPTH (m)	Soil description in accordance with the NZ Geotechnical Society Inc 2005 "Guidelines for Field Description of Soil and Rock in Engineering Use"			WATER LEVEL (m)		DEPTH (m)	LABORATORY TESTS	
Fill	0.0		SILT, trace to minor fine to medium sub-rounded to rounded gravel, trace fine sand, brown, loose to medium dense, dry to moist, non-plastic					SCALA PENETROMETER TEST METHOD NZS4402: 1986 test 6.5.2 (Blows/100mm)		
			minor to some sub rounded to rounded gravel							
Alluvial Deposits	0.5		Sandy fine to coarse sub-rounded to rounded GRAVEL, trace to minor silt, trace sub-rounded to rounded cobble, greyish brown, dense to very dense, moist					0.5		
			trace silt							
	1.0		trace to minor sub-rounded to rounded cobble					1.0		
			moist to wet							
	1.5							1.5		
			wet							
	2.0							2.0		
	2.5							2.5		
	3.0							3.0		
			END OF TEST PIT. 3.0 METRES. [Target Depth]							
			COMMENTS:							

TEST PIT LOG C14652_TP1-10.GPJ S+R 2012-AGS - REVISED.GDT 18/12/14

 Soil & Rock Consultants GEOTECHNICAL & ENVIRONMENTAL ENGINEERS			CLIENT: Lincoln Amor PROJECT: 847 Jones Rd, Rolleston			Test Pit No: TP07 Sheet 1 of 1			
Drill Type: 8t Excavator Drilled By: Soil & Rock Consultants Date Started: 16/12/14 Date Finished: 16/12/14			Project No: C14652 Coordinates: 1549587 E, 5173527 N Ground Elevation: 55m LINZ Topo Water Level: Groundwater not encountered			Logged By: MG Reviewed By: MLB Surface Conditions: Near level, grass Shear Vane Number: N/A			
STRATIGRAPHY	DEPTH (m)	GRAPHIC LOG	Soil description in accordance with the NZ Geotechnical Society Inc 2005 "Guidelines for Field Description of Soil and Rock in Engineering Use"			WATER LEVEL (m)	DEPTH (m)	SCALA PENETROMETER TEST METHOD NZS4402: 1986 test 6.5.2 (Blows/100mm)	LABORATORY TESTS
Fill	0.0		SILT, trace fine to medium sub-rounded to rounded gravel, trace fine sand, brown, dense, dry to moist, non-plastic				0.0		
	0.5		Silty fine to coarse sub-rounded to rounded GRAVEL, trace to minor fine sand, greyish brown, dense to very dense, dry to moist				0.5		
Alluvial Deposits	1.0		Sandy fine to coarse sub-rounded to rounded GRAVEL, trace cobble, trace silt, greyish brown, dense to very dense, moist				1.0		
	1.5		moist to wet				1.5		
	2.0		wet				2.0		
	2.5		trace to minor sub rounded cobble				2.5		
	3.0		trace sub rounded to rounded cobble				3.0		
			END OF TEST PIT. 2.8 METRES. [Target Depth]						
COMMENTS:									

TEST PIT LOG C14652_TP1-10.GPJ S+R 2012-AGS - REVISED.GDT 18/12/14

WATER



Water level on date shown

METHOD (shows drilling method)

OB	open barrel
Wash	wash boring
TT	triple tube
UT	thin walled undisturbed tube
SPT	standard penetration test – open nose sampler
Nc	standard penetration test – solid nose sampler
MA	machine auger
PS	piston sample
PCT	percussion – top drive
PCB	percussion – bottom drive
Conc	concentrics
Sonic	sonic
HA	hand auger
VE	vacuum excavation

SAMPLES

Dx	Disturbed sample, number x
Bx	Bulk sample, number x
Ux(d)	Undisturbed sample, number x, tube diameter d in mm
Wx	Water sample, number x

MOISTURE

Dry, looks and feels dry
Moist, no free water on hand when remoulding
Wet, free water on hand when remoulding
Saturated, soil below water table

SOIL AND ROCK DESCRIPTIONS

CONSISTENCY

Cohesive Soils	Undrained Shear Strength (kPa)
Very soft	<12
Soft	12 to 25
Firm	25 to 50
Stiff	50 to 100
Very stiff	100 to 200
Hard	>200

Soil and Rock Descriptions are generally as described in the NZ Geotechnical Society "Field Description of Soil and Rock – Guideline for the Field Classification and Description of Soil and Rock for Engineering Purposes", dated December 2005.

Vane Shear Strength measurements in accordance with the NZ Geotechnical Society "Guideline for hand held shear vane test" dated August 2001.

IN SITU TESTS

SV	= 40/10	In situ shear strength and remoulded shear strength respectively, as measured by Geotechnics/ Pilcon Shear Vane
τ	= 50/12	Vane shear strength and remoulded vane shear strength respectively, corrected to BS1377
UTP	=	Unable To Penetrate with Shear Vane
N	= 15	SPT uncorrected blow count for 300mm penetration
N _c	= 50+	SPT uncorrected blow count for 300 mm penetration using solid nose sampler

★

AL	Atterberg limits
UU	Unconsolidated undrained triaxial
PSD	Particle size
CU	Consolidated undrained triaxial
CONS	Consolidation
COMP	Compaction
UCS	Unconfined compression

WEATHERING

CW	Completely weathered
HW	Highly weathered
MW	Moderately weathered
SW	Slightly weathered
UW	Unweathered

GRAPHIC LOG (1 or a combination of the following)



Fill



Silt



Cobbles



Sandstone



Fine igneous



Core loss



Sand



Boulders



Limestone



Coarse igneous



Organics



Shells



Mudstone



Schist



Clay



Gravel



Siltstone



Basalt

ORGANIC SOILS

Von Post Degree of Humification

H1	Completely unconverted and mud-free peat, when pressed gives clear water and plant structure is visible.
H2	Practically unconverted and mud-free peat, when pressed gives almost clear water and plant structure is visible.
H3	Very slightly decomposed or very slightly muddy peat, when pressed gives marked muddy water, no peat substance passes through the fingers and plant structure is less visible.
H4	Slightly decomposed or slightly muddy peat, when pressed gives marked muddy water and plant structure is less visible.
H5	Moderately decomposed or very muddy peat with growth structure evident but slightly obliterated.
H6	Moderately decomposed or very muddy peat with indistinct growth structure.
H7	Fairly well decomposed or very muddy peat but the growth structure can just be seen.
H8	Well decomposed or very muddy peat with very indistinct growth structure.
H9	Practically decomposed or mud-like peat in which almost no growth structure is evident.
H10	Completely decomposed or mud peat where no growth structure can be seen, entire substance passes through the fingers when pressed.



TEST PIT LOG

PROJECT: Walkers Rd Widening DD			JOB NUMBER: 3335348/400		
SITE LOCATION: Walkers Road, Rolleston			CLIENT: Selwyn District Council (SDC)		
CIRCUIT: NZTM2000		TEST PIT LOCATION: West side of Walkers Rd - near the corner with Runners Rd			
COORDINATES: N 5,172,311 m		R L: 59 m		COORDINATE ORIGIN: hhGPS	
E 1,547,620 m		DATUM: NZVD		ACCURACY: ±5m	

DEPTH (m)	SAMPLES	GRAPHIC LOG	SOIL / ROCK DESCRIPTION	GEOLOGICAL UNIT	SV	γ (kPa)	WATER LEVEL	R L (m)
0.5	B1		Soft fine to coarse sandy SILT, minor organics; brown; moist, non-plastic. Organics: rootlets. [TOPSOIL].	Quaternary Alluvium				58.5
			Stiff fine to coarse sandy SILT, some fine to coarse gravels, trace organics, trace cobbles; brown; moist, non-plastic. Gravel/ Cobbles: rounded to well-rounded, slightly weathered, greywacke. Organics: rootlets.					
			Tightly packed cobbly fine to coarse GRAVEL, some fine to coarse SAND, minor silt, trace organics; brown; moist, well graded. Gravel/ Cobbles: subrounded to rounded, slightly weathered, greywacke. Organics: rootlets.					
			From 0.80m: no organics.					
1.0								58.0
1.5								57.5
2.0			END OF LOG @ 2 m					57.0
2.5								56.5
3.0								56.0
3.5								55.5
4.0								55.0
4.5								54.5

DATE EXCAVATED: 28/10/20	CONTRACTOR: HEB Construction	COMMENTS: Test pit terminated at target depth. Test pit wall stability good. Groundwater not encountered. Coordinates obtained using a handheld GPS.
LOGGED BY: VVC	EQUIPMENT: Hydrovacuum	
SHEAR VANE No: N/A	METHOD: WB	

FOR EXPLANATION OF SYMBOLS AND ABBREVIATIONS SEE KEY SHEET

WATER



Water level on date shown

METHOD (shows drilling method)

OB	open barrel
Wash	wash boring
TT	triple tube
UT	thin walled undisturbed tube
SPT	standard penetration test – open nose sampler
Nc	standard penetration test – solid nose sampler
MA	machine auger
PS	piston sample
PCT	percussion – top drive
PCB	percussion – bottom drive
Conc	concentrics
Sonic	sonic
HA	hand auger
VE	vacuum excavation

SAMPLES

Dx	Disturbed sample, number x
Bx	Bulk sample, number x
Ux(d)	Undisturbed sample, number x, tube diameter d in mm
Wx	Water sample, number x

MOISTURE

Dry, looks and feels dry
Moist, no free water on hand when remoulding
Wet, free water on hand when remoulding
Saturated, soil below water table

SOIL AND ROCK DESCRIPTIONS

CONSISTENCY

Cohesive Soils	Undrained Shear Strength (kPa)
Very soft	<12
Soft	12 to 25
Firm	25 to 50
Stiff	50 to 100
Very stiff	100 to 200
Hard	>200

Soil and Rock Descriptions are generally as described in the NZ Geotechnical Society "Field Description of Soil and Rock – Guideline for the Field Classification and Description of Soil and Rock for Engineering Purposes", dated December 2005.

Vane Shear Strength measurements in accordance with the NZ Geotechnical Society "Guideline for hand held shear vane test" dated August 2001.

IN SITU TESTS

SV	= 40/10	In situ shear strength and remoulded shear strength respectively, as measured by Geotechnics/ Pilcon Shear Vane
τ	= 50/12	Vane shear strength and remoulded vane shear strength respectively, corrected to BS1377
UTP	=	Unable To Penetrate with Shear Vane
N	= 15	SPT uncorrected blow count for 300mm penetration
N _c	= 50+	SPT uncorrected blow count for 300 mm penetration using solid nose sampler

★

AL	Atterberg limits
UU	Unconsolidated undrained triaxial
PSD	Particle size
CU	Consolidated undrained triaxial
CONS	Consolidation
COMP	Compaction
UCS	Unconfined compression

WEATHERING

CW	Completely weathered
HW	Highly weathered
MW	Moderately weathered
SW	Slightly weathered
UW	Unweathered

GRAPHIC LOG (1 or a combination of the following)



Fill



Silt



Cobbles



Sandstone



Fine igneous



Core loss



Sand



Boulders



Limestone



Coarse igneous



Organics



Shells



Mudstone



Schist



Clay



Gravel



Siltstone



Basalt

ORGANIC SOILS

Von Post Degree of Humification

H1	Completely unconverted and mud-free peat, when pressed gives clear water and plant structure is visible.
H2	Practically unconverted and mud-free peat, when pressed gives almost clear water and plant structure is visible.
H3	Very slightly decomposed or very slightly muddy peat, when pressed gives marked muddy water, no peat substance passes through the fingers and plant structure is less visible.
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H7	Fairly well decomposed or very muddy peat but the growth structure can just be seen.
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H9	Practically decomposed or mud-like peat in which almost no growth structure is evident.
H10	Completely decomposed or mud peat where no growth structure can be seen, entire substance passes through the fingers when pressed.



TEST PIT LOG

SHEET 1 of 1

PROJECT: Walkers Rd Widening DD			JOB NUMBER: 3335348/400		
SITE LOCATION: Walkers Road, Rolleston			CLIENT: Selwyn District Council (SDC)		
CIRCUIT: NZTM2000		TEST PIT LOCATION: East side of Walkers Rd - between Runners Rd and the rail track			
COORDINATES: N 5,172,266 m		R L: 59 m		COORDINATE ORIGIN: hhGPS	
E 1,547,662 m		DATUM: NZVD		ACCURACY: ±5m	

DEPTH (m)	SAMPLES	GRAPHIC LOG	SOIL / ROCK DESCRIPTION	GEOLOGICAL UNIT	SV	τ (kPa)	WATER LEVEL	R L (m)
			Stiff fine sandy SILT, trace organics; brown; moist, non-plastic. Organics: rootlets. [TOPSOIL]	Quaternary Alluvium				
0.5			Firm fine to medium sandy SILT, some fine to coarse gravel, trace cobbles, trace organics; brown; moist, non-plastic. Gravel/ Cobbles: subrounded to well-rounded, slightly weathered, greywacke. Organics: rootlets.					58.5
1.0	B2		Tightly packed cobbly fine to coarse GRAVEL, some fine to coarse SAND, minor silt; brown; moist, well graded. Gravel/ Cobbles: subrounded to well-rounded, slightly weathered, greywacke.					58.0
1.5								57.5
2.0			END OF LOG @ 2 m					57.0
2.5								56.5
3.0								56.0
3.5								55.5
4.0								55.0
4.5								54.5

DATE EXCAVATED: 28/10/20	CONTRACTOR: HEB Construction	COMMENTS: Test pit terminated at target depth. Test pit wall stability good. Groundwater not encountered. Coordinates obtained using a handheld GPS.
LOGGED BY: DD	EQUIPMENT: Hydrovacuum	
SHEAR VANE No: N/A	METHOD: WB	

FOR EXPLANATION OF SYMBOLS AND ABBREVIATIONS SEE KEY SHEET

BECA LIB 1.07.3.GLB Log BECA TEST PIT WALKERS RD TEST PITS.GPJ <<DrawingFile>> 06/11/2020 17:05 8.30.004 D:\git\Lab and in Situ Tools - DGD\ Lib\ Beca 1.07.2 2015\07\31 Proj\ Beca 1.07 2014\12\16

WATER



Water level on date shown

METHOD (shows drilling method)

OB	open barrel
Wash	wash boring
TT	triple tube
UT	thin walled undisturbed tube
SPT	standard penetration test – open nose sampler
Nc	standard penetration test – solid nose sampler
MA	machine auger
PS	piston sample
PCT	percussion – top drive
PCB	percussion – bottom drive
Conc	concentrics
Sonic	sonic
HA	hand auger
VE	vacuum excavation

SAMPLES

Dx	Disturbed sample, number x
Bx	Bulk sample, number x
Ux(d)	Undisturbed sample, number x, tube diameter d in mm
Wx	Water sample, number x

MOISTURE

Dry, looks and feels dry
Moist, no free water on hand when remoulding
Wet, free water on hand when remoulding
Saturated, soil below water table

SOIL AND ROCK DESCRIPTIONS

CONSISTENCY

Cohesive Soils	Undrained Shear Strength (kPa)
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WEATHERING

CW	Completely weathered
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GRAPHIC LOG (1 or a combination of the following)



Fill



Silt



Cobbles



Sandstone



Fine igneous



Core loss



Sand



Boulders



Limestone



Coarse igneous



Organics



Shells



Mudstone



Schist



Clay



Gravel



Siltstone



Basalt

ORGANIC SOILS

Von Post Degree of Humification

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H2	Practically unconverted and mud-free peat, when pressed gives almost clear water and plant structure is visible.
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H10	Completely decomposed or mud peat where no growth structure can be seen, entire substance passes through the fingers when pressed.



TEST PIT LOG

SHEET 1 of 1

PROJECT: Walkers Rd Widening DD			JOB NUMBER: 3335348/400		
SITE LOCATION: Walkers Road, Rolleston			CLIENT: Selwyn District Council (SDC)		
CIRCUIT: NZTM2000		TEST PIT LOCATION: East side of Walkers Rd - next to the farm access gate			
COORDINATES: N 5,172,558 m		R L: 61 m		COORDINATE ORIGIN: hhGPS	
E 1,547,492 m		DATUM: NZVD		ACCURACY: ±5m	

DEPTH (m)	SAMPLES	GRAPHIC LOG	SOIL / ROCK DESCRIPTION	GEOLOGICAL UNIT	SV	γ (kPa)	WATER LEVEL	R L (m)
0.5	B3		Soft fine to coarse sandy SILT, minor organics, trace fine gravel; brown; moist, non-plastic. Organics: rootlets. Gravel: subangular, slightly weathered, greywacke. [TOPSOIL]	Quaternary Alluvium				60.5
			Stiff fine to coarse sandy SILT, some fine to coarse gravel, trace organics, trace cobbles; brown; moist, non-plastic. Gravel/ Cobbles: rounded to well-rounded, slightly weathered, greywacke. Organics: rootlets.					
			Tightly packed fine to coarse gravelly COBBLES, some fine to coarse sand, minor silt, trace organics; brown; moist, well graded. Gravel/ Cobbles: rounded, slightly weathered, greywacke. Organics: rootlets.					
1.0			From 1.0m: no organics.					60.0
1.5								59.5
2.0			END OF LOG @ 2 m					59.0
2.5								58.5
3.0								58.0
3.5								57.5
4.0								57.0
4.5								56.5

DATE EXCAVATED: 29/10/20	CONTRACTOR: HEB Construction	COMMENTS: Test pit terminated at target depth. Test pit wall stability good. Groundwater not encountered. Coordinates obtained using a handheld GPS.
LOGGED BY: VVC	EQUIPMENT: Hydrovacuum	
SHEAR VANE No: N/A	METHOD: WB	

FOR EXPLANATION OF SYMBOLS AND ABBREVIATIONS SEE KEY SHEET

BECA LIB 1.07.3.GLB Log BECA TEST PIT WALKERS RD TEST PITS.GPJ <<DrawingFile>> 06/11/2020 17:05 8.30.004 D:\git\Lab and In Situ Tools\DOG\Lib\Beca 1.07.2 2015-07-31 Proj\Beca 1.07.2014-12-16

A4 Scale 1:25

Borelog for well M36/0026

Grid Reference (NZTM): 1549008 mE, 5172830 mN
Location Accuracy: 2 - 15m
Ground Level Altitude: 55.8 m +MSD Accuracy: < 0.5 m
Driller: McMillan T T
Drill Method: Cable Tool
Borelog Depth: 56.1 m Drill Date: 07-Jan-1971



Scale(m)	Water Level	Depth(m)	Full Drillers Description	Formation Code
		0.30m	Earth and clay	
		0.30m	Earth and clay Clay and gravel	
		1.80m	Clay and gravel	
		1.80m	Open large and small gravels	
		6.69m	Open large and small gravels	
		6.69m	Gravel, clay and sand	
		11.90m	Gravel, clay and sand	
		11.90m	Open gravels	
		13.70m	Open gravels	
		13.70m	Slightly claybound gravels	
		16.20m	Slightly claybound gravels	
		16.20m	Claybound gravels	
		20.70m	Claybound gravels	
		20.70m	Gravel, clay and sand	
		22.60m	Gravel, clay and sand	
		22.60m	Broken claybound gravels	
		28.29m	Broken claybound gravels	
		28.29m	Medium Brown gravels and sand	
		29.00m	Medium Brown gravels and sand	
		29.00m	Large broken gravels	
		30.50m	Large broken gravels	
		30.50m	Brown gravel, sand and clay	
		34.09m	Brown gravel, sand and clay	
		34.09m	Claybound gravels	
		36.59m	Claybound gravels	
		36.59m	Small to medium Brown gravels	
		37.79m	Small to medium Brown gravels	
		37.79m	Very sandy small gravels and thick claywash	
		39.29m	Very sandy small gravels and thick claywash	
		39.29m	Gravel sand and clay	
		46.59m	Gravel sand and clay	
		46.59m	Gravel sand and claywash	
		51.79m	Gravel sand and claywash	
		51.79m	Gravel, sand and thick claywash	
		54.90m	Gravel, sand and thick claywash	
		54.90m	Gravel clay and sand	
		56.09m		
		56.09m		

Borelog for well M36/0030

Grid Reference (NZTM): 1547355 mE, 5172595 mN

Location Accuracy: 2 - 15m

Ground Level Altitude: 58.9 m +MSD Accuracy: < 0.5 m

Driller: Ministry of Works

Drill Method: Cable Tool

Borelog Depth: 55.5 m Drill Date: 06-Nov-1974



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	Scale(m)	Water Level	Depth(m)	Full Drillers Description	Formation Code
				Silty sandy Grey/Brown gravel	
			2.09m 2.09m	Silty sandy Grey/Brown gravel Sandy Grey gravel	
			7.90m 7.90m	Sandy Grey gravel Sandy Grey/Brown gravel, some silt	
11					
			19.50m 19.50m 20.10m 20.10m	Sandy Grey/Brown gravel, some silt Coarse Grey/Brown gravel, stained Coarse Grey/Brown gravel, stained Silty sandy Grey/Brown gravel	
22			24.40m 24.40m	Silty sandy Grey/Brown gravel Sandy Grey/Brown gravel	
			29.90m 29.90m	Sandy Grey/Brown gravel Sandy Grey/Brown gravel, some silt, Brown stained	
33					
44					
			55.50m		

Borelog for well M36/0084

Grid Reference (NZTM): 1548628 mE, 5173180 mN

Location Accuracy: 50 - 300m

Ground Level Altitude: 58.2 m +MSD Accuracy: < 0.5 m

Driller: A M Bislev & Co

Drill Method: Cable Tool

Borelog Depth: 35.0 m Drill Date: 17-Jun-1980



Scale(m)	Water Level	Depth(m)	Full Drillers Description	Formation Code
			Soil	
		0.60m	Soil	
		0.60m	Brown clay	
		1.50m	Brown clay	
		1.50m	Medium Brown gravel	
5				
10		9.50m	Medium Brown gravel	
		9.50m	Brown clay	
15		14.90m	Brown clay	
		14.90m	Fine Brown gravel	
		15.50m	Fine Brown gravel	
		15.50m	Clay and Brown gravel	
20				
		21.60m	Clay and Brown gravel	
		21.60m	Fine to medium Brown gravel	
25		25.90m	Fine to medium Brown gravel	
		25.90m	Clay and medium Brown gravel	
30		29.90m	Clay and medium Brown gravel	
		29.90m	Fine Brown gravel	
		35.00m		

Borelog for well M36/3064

Grid Reference (NZTM): 1548688 mE, 5173350 mN

Location Accuracy: 2 - 15m

Ground Level Altitude: 59.0 m +MSD Accuracy: < 0.5 m

Driller: A M Bisley & Co

Drill Method: Cable Tool

Borelog Depth: 55.4 m Drill Date: 05-Aug-1985

[illegible]

Borelog for well M36/4984

Grid Reference (NZTM): 1547598 mE, 5173010 mN
 Location Accuracy: 2 - 15m
 Ground Level Altitude: 60.0 m +MSD Accuracy: < 2.5 m
 Driller: McMillan Drilling Ltd
 Drill Method: Unknown
 Borelog Depth: 54.0 m Drill Date: 30-May-1997

Scale(m)	Water Level	Depth(m)	Full Drillers Description	Formation Code
		0.30m	Earth Sandy claybound gravel	
11		11.00m	Moist sandy claybound gravel	
22		23.70m	Water-bearing lightly stained sandy gravel with clay	
32		46.00m	Water-bearing sandy gravel with clay	
43		54.00m		

Borelog for well M36/4985

Grid Reference (NZTM): 1547938 mE, 5173140 mN
 Location Accuracy: 10 - 50m
 Ground Level Altitude: 60.5 m +MSD Accuracy: < 0.5 m
 Driller: McMillan Drilling Ltd
 Drill Method: Unknown
 Borelog Depth: 48.0 m Drill Date: 04-Jun-1997

Scale(m)	Water Level	Depth(m)	Full Drillers Description	Formation Code
		0.30m	Earth	
		0.30m	Earth	
			Sandy claybound gravel	
5				
		10.00m		
10		10.00m	Sandy claybound gravel	
			Moist sandy claybound gravel	
15				
		23.70m		
25		23.70m	Moist sandy claybound gravel	
			Water-bearing sandy gravel with clay	
30				
		35.20m		
35		35.20m	Water-bearing sandy gravel with clay	
			Water-bearing lightly stained sandy gravel with clay	
40				
		48.00m		

Borelog for well M36/4986

Grid Reference (NZTM): 1548099 mE, 5173143 mN

Location Accuracy: 2 - 15m

Ground Level Altitude: 59.8 m +MSD Accuracy: < 0.5 m

Driller: McMillan Drilling Ltd

Drill Method: Unknown

Borelog Depth: 48.0 m Drill Date: 01-May-1997



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Scale(m)	Water Level	Depth(m)	Full Drillers Description	Formation Code
		0.30m	Earth	
		0.30m	Earth	
			Grey sandy gravel	
		3.70m	Grey sandy gravel	
5		3.70m	Sandy claybound gravel	
10				
15		15.00m	Sandy claybound gravel	
		15.00m	Moist sandy claybound gravel	
20				
25		23.60m	Moist sandy claybound gravel	
		23.60m	Water-bearing sandy gravel and clay	
30		29.00m	Water-bearing sandy gravel and clay	
		29.00m	Water-bearing lightly stained sandy gravel with clay	
35				
40				
45				
		48.00m		

Grid Reference (NZTM): 1547289 mE, 5172950 mN
Location Accuracy: 50 - 300m
Ground Level Altitude: 61.8 m +MSD Accuracy: < 0.5 m
Driller: Smiths Welldrilling
Drill Method: Rotary Rig
Borelog Depth: 43.0 m Drill Date: 21-Aug-1996

[illegible]

Borelog for well M36/5139

Grid Reference (NZTM): 1548878 mE, 5173390 mN

Location Accuracy: 50 - 300m

Ground Level Altitude: 58.3 m +MSD Accuracy: < 0.5 m

Driller: Smiths Welldrilling

Drill Method: Rotary/Percussion

Borelog Depth: 39.5 m Drill Date: 19-Aug-1996

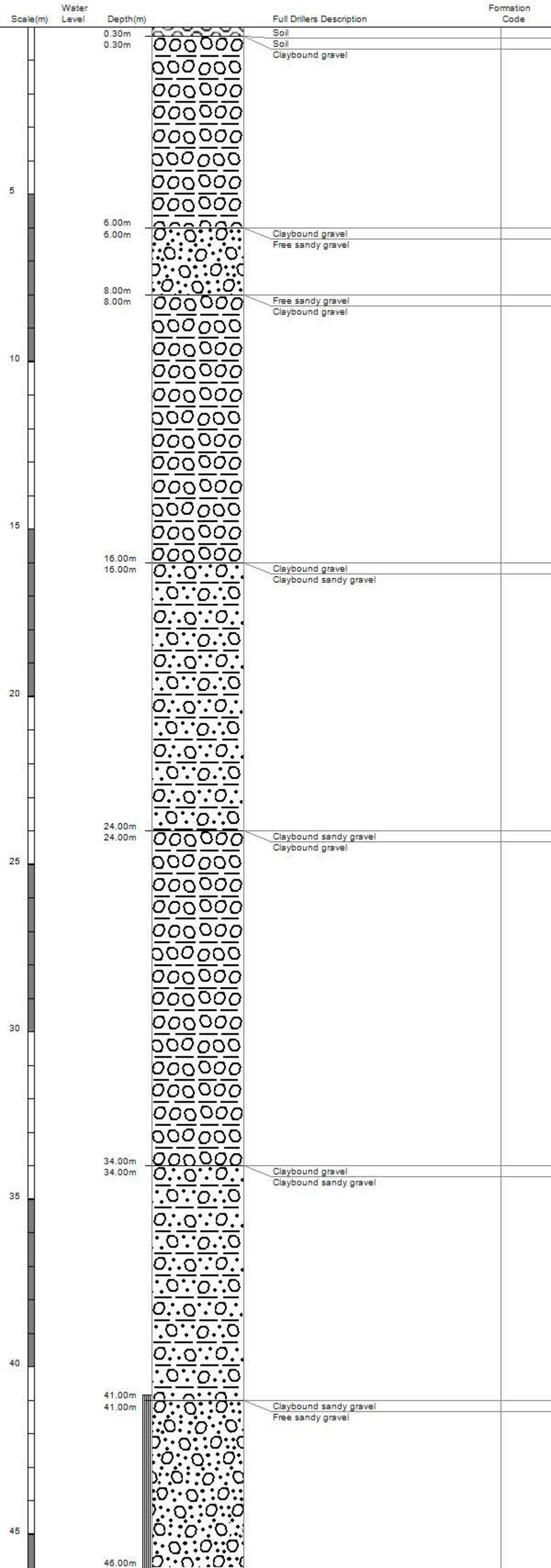


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Scale(m)	Water Level	Depth(m)	Full Drillers Description	Formation Code
		1.00m	Soil	
		1.00m	Soil	
			Claybound gravel	
5				
10				
		12.00m	Claybound gravel	
		12.00m	Free sandy gravel	
15				
		16.00m	Free sandy gravel	
		16.00m	Claybound gravel	
20				
25				
		25.00m	Claybound gravel	
		25.00m	Sandy claybound gravel	
30				
		33.00m	Sandy claybound gravel	
		33.00m	Free sandy gravel	
35				
		39.50m		

Borelog for well M36/5330

Grid Reference (NZTM): 1547468 mE, 5172960 mN
Location Accuracy: 50 - 300m
Ground Level Altitude: 61.0 m +MSD Accuracy: < 0.5 m
Driller: Smiths Welldrilling
Drill Method: Rotary Rig
Borelog Depth: 46.0 m Drill Date: 27-Aug-1997



Borelog for well M36/5525

Grid Reference (NZTM): 1547518 mE, 5172810 mN

Location Accuracy: 50 - 300m

Ground Level Altitude: 59.6 m +MSD Accuracy: < 0.5 m

Driller: Smiths Welldrilling

Drill Method: Rotary Rig

Borelog Depth: 47.0 m Drill Date: 28-Feb-1998



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Scale(m)	Water Level	Depth(m)		Full Drillers Description	Formation Code	
5		0.20m		Soil		
		0.20m		Soil		
				Claybound gravel		
		4.50m		Claybound gravel		
		4.50m		Large gravel		
		6.50m			Large gravel	
		6.50m	Claybound gravel			
	10					
15			15.00m		Claybound gravel	
		15.00m	Free sandy gravel			
	20		22.00m		Free sandy gravel	
		22.00m	Claybound sandy gravel			
25						
	30					
35						
	40					
45			43.00m		Claybound sandy gravel	
		43.00m	Free sandy gravel			
			47.00m			